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## INSTRUCTION MANUAL

## MODEL 2002A

## SWEEP/SIGNAL GENERATOR


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## SCOPE OF THIS MANUAL

This manual provides descriptive material and instructions for the installation, operation, maintenance, and repair of the WAVETEK Model 2002A Sweep/Signal Generator.

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### 1.1 INTRODUCTION

The Model 2002A covers the 1 to 2500 MHz range in three bands. Band 1 is covered by a 1 to 500 MHz heterodyne sweep oscillator. Band 2 is covered by two fundamental oscillators which sweep from 500 to 1000 MHz and 1000 to 1500 MHz , respectively. Band 3 is covered by a single fundamental oscillator sweeping from 1500 to 2500 MHz . Additionally, all four oscillators may be stacked (sequentially swept) to cover the entire 1 to 2500 MHz instrument range (band 4).

Each of the four frequency bands ( $1-500 \mathrm{MHz}, 500-1500$ $\mathrm{MHz}, 1500-2500 \mathrm{MHz}$, and 1-2500 MHz) may be used in three modes of operation: start/stop, $\Delta \mathrm{f}$, or CW. It can be swept over any portion of a given band, in either direction, at any rate from 50 sweeps per second to 1 sweep every 100 seconds. Manual, triggered, or recurring sweeps are provided. The sweep frequency, sweep width, and output attenuation may be controlled by external voltages.

Other features of the Model 2002A include a SLOPE control which compensates for frequency dependent variations in the external circuitry, and a 1 kHz square-wave modulator for low-level recovery applications.

This instrument also includes an elaborate frequency marker system. Up to five crystal-controlled birdy marker modules (single frequency or harmonic type) may be plugged into the Model 2002A. Each module has its own front-panel on/off switch. Additionally, a single module producing harmonic markers at $1,10,50$, and 100 MHz intervals may be installed. Front-panel SIZE and WIDTH controls enable optimum adjustment of the marker display. The marker system features dual-amplitude markers for easy identification. In application, the markers may be tilted up to $90^{\circ}$ for easy viewing when displayed with steep transition signals, or they may be rectified by a front-panel switch for $X-Y$ plotter applications.

Other optional features include a rear-panel Auxilliary RF Output and a Pen Lift circuit for use with X-Y plotters.

Most optional features, as well as the functional circuits for the basic sweep generator, have modular plug-in construction. This allows optional features to be factory installed at the time of purchase, or customer installed at a later date. This concept offers protection against obsolesence, since updated and additional features can be simply and economically added as new test procedures dictate. In addition, maintenance problems can be greatly simplified by stocking several modules instead of hundreds of discrete components.

### 1.2 SPECIFICATIONS

1.2.1 FREOUENCY

RANGE

SWEEP WIDTH

ACCURACY AT $25^{\circ} \mathrm{C}$

Band 1
Bands 2, 3
Band 4

ACCURACY VS TEMP
Bands 1, 2
Band 3

DISPLAY LINEARITY

BAND SWITCHING

## SPURIOUS SIGNALS

HARMONICS

NON-HARMONICS

RESIDUAL FM (CW MODE)

DRIFT

BLANKING

> 1 to 2500 MHz in four bands:
> $1-500 / 500-1500 / 1500-2500 / 1-2500$
$\Delta f-200 \mathrm{kHz}$ to 500 MHz on all bands

## S/S - 200 kHz to 500 MHz on band 1 200 kHz to 1000 MHz on bands 2, 3 1 MHz to 2500 MHz on band 4

CW


CENT FREO SWP WIDTH

| 10 | 10 | 15 | 15 MHz |
| :--- | :--- | :--- | :--- |
| 20 | 20 | 30 | 30 MHz |
| 50 | 50 | 50 | 50 MHz |

## $500 \mathrm{kHz} /{ }^{\circ} \mathrm{C}$ <br> $1 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$

Frequency scale calibrated in 10 MHz increments for band $1,20 \mathrm{MHz}$ increments for bands 2 and 3 , and 50 MHz for band 4. $\Delta f$ sweep width is calibrated in 10 MHz intervals.

1\% (discounting band switch discontinuities)

Band switching discontinuity points occur at 500,1000 , and 1500 MHz . The discontinuity is $-9+20 \mathrm{MHz}$. A band switching blanking output signal (approximately 15 V in magnitude, switchable polarity) occurs at the rear-panel BAND STACKING BLANKING output connector.

| SIGNAL FREQUENCY | SPURIOUS SIGNAL LEVEL |
| :--- | :--- |
| 1 to 10 MHz | -20 dBc |
| 10 to 2500 MHz | -30 dBc |
| 1 to 500 MHz | $-35 \mathrm{dBc}(1 \mathrm{to} 500 \mathrm{MHz})$ |
| 1 to 500 MHz | -30 dBc (full range) |
| 500 to 2500 MHz | non detectable |
|  |  |
| Bands 1,2 | $<10 \mathrm{kHz}$ peak to peak |
| Band 3 | $<20 \mathrm{kHz}$ peak to peak |
|  |  |
| Bands 1,2 | $<100 \mathrm{kHz} / 5 \mathrm{~min}$. |
|  | $<2 \mathrm{MHz} / 8 \mathrm{hr}$. |
| Band 3 | $<200 \mathrm{kHz} / 5 \mathrm{~min}$. |
|  | $<4 \mathrm{MHz} / 8 \mathrm{hr}$. |

(At constant temperature after 1 hr . warm-up, and allowing a 5 minute stabilizing period after a frequency change.)

A front-panel switch enables the RF output to be removed during the sweep retrace time to provide a zero volt base line.

IMPEDANCE

SWR

MAXIMUM LEVEL

ATTENUATION

ACCURACY

FLATNESS AT +13 dBm OUTPUT
SLOPE

OUTPUT CONNECTOR

EXTERNAL LEVELING
1.2.3 SWEEP

## OPERATING MODES

SWEEP MODES

SWEEP TIME

SWEEP DWELL

HORIZONTAL OUTPUT

## 50 ohms

Less than 1.5:1 with insertion loss of 10 dB from STEP ATTENUATOR. Less than 1.3:1 with insertion of 20 dB or more from STEP ATTENUATOR.
$+13 \mathrm{dBm}$

Output continuously adjustable from +13 to -77 dBm .70 dB in 10 dB steps plus a 20 dB vernier.

STEP ATTENUATOR: 3\% of attenuation (maximum error at $70 \mathrm{~dB}= \pm 2.1 \mathrm{~dB})$.
VERNIER ATTENUATOR: $\pm .5 \mathrm{~dB}$ over top 13 dB of range, lower 7 dB is unspecified.
$\pm 0.5 \mathrm{~dB}$

Up to $\pm 1 \mathrm{~dB} / \mathrm{GHz}$ of slope may be imposed on the RF output via the front-panel SLOPE control. The reference (pivot point) of this slope is 1 MHz . The output METER will indicate the change in output level at slow sweep rates. NOTE: The OUTPUT VERNIER must be set so that the added slope will not produce an RF output level greater than the highest possible OUTPUT VERNIER setting.

Type N

An external negative monitor signal, between .2 and 2 volts, may be used to level the RF output.

Start/Stop - $\Delta \mathbf{f}$ - CW

Repetitive sweep
Single sweep
Externally triggered sweep
Manual sweep
Line-locked sweep
Continuously variable from less than .01 to more than 100 seconds per sweep in four decade ranges with vernier (add 1 msec for every band switch point crossed). Manual and line-locked sweep are also provided. NOTE: In line-locked sweep, the sweep time for band 4 is double that for bands 1,2 , and 3.

Approximately 4 msec delay at start of sweep controlled by rear-panel switch.

Zero to +10 volts. Impedance $10 \mathrm{k} \Omega$.

### 1.2.4 MODULATION

### 1.2.5 MARKER SPECIFICATIONS

TYPE

EXTERNAL

## INTERNAL

Single Frequency

Harmonic (comb)

ACCURACY

WIDTH

SIZE

DUAL AMPLITUDE FEATURE

Square-wave modulation produces blanking of RF output at a 1 kHz rate for low-level recovery operations. On/off control is provided on the front panel.

For external AM and FM, refer to Section 1.2.6, Remote Programming.

Birdy by-pass
Front-panel BNC connector accepts external CW signal for conversion to a birdy marker. Input level: 100 mV into 50 ohms. Front-panel on/off control is provided.

The instrument has provisions for either single frequency or harmonic type plug-in birdy marker modules. Maximum of five A1 or A2 options and one A3 option.

A1 options are individually controlled by front-panel push buttons.

A2 or A3 options provide markers at multiples of the specified fundamental frequency.

A2 options produce harmonics of one crystal frequency and are individually controlled by front-panel push buttons.

A3 option is a combination $1,10,50$, and 100 MHz harmonic marker controlled by a front-panel rotary switch.

| Option A1 or A2 | $.005 \%$ at $25^{\circ} \mathrm{C}$ |
| :--- | :--- |
|  | $.007 \%, 0^{\circ}$ to $50^{\circ} \mathrm{C}$ |
| Option A3 | $.005 \%, 0^{\circ}$ to $50^{\circ} \mathrm{C}$ |

Adjustable in four steps from approximately 15 to 400 kHz .

The instrument is capable of providing markers at two distinct amplitudes to facilitate marker identification. An internal adjustment controls the ratio of the two sizes.

Markers controlled by front-panel buttons a, b, c, and EXT (first, second, third, and sixth from left) are full-size, whereas markers controlled by buttons $d$ and $e$ can be set for some fraction of this size.

This feature pertains to the Deluxe Harmonic Marker (Option A3) in the following manner.

| Setting | Reducible | Full size |
| ---: | :---: | ---: |
| 1 | 1 MHz | 10 MHz |
| 10 | 10 MHz | 100 MHz |
| 50 | 50 MHz | 100 MHz |
| 100 | --- | 100 MHz |

## AMPLITUDE CONTROL

## RECTIFICATION

TILT
1.2.6 REMOTE PROGRAMMING

BAND SELECTION FREQUENCY

## SWEEP WIDTH

VERNIER, 0-20 dB OUTPUT

EXTERNAL AM

All markers are continuously adjustable with front-panel controls over two ranges. The ranges for full-size markers are: 4 Vpp to 10 mVpp and 25 mVpp to $50 \mu \mathrm{Vpp}$. (Voltages are approximate.)

Birdy markers can be rectified (positive) for use with X-Y plotters. Size varies with detector's impedance. Adjustable from approximately 2 V to 1 mV with detector impedance of 1 Megohm, or from 0.2 V to 1 mV with detector impedance of 0 ohms.

This feature adds to the normally vertical marker a horizontal component with an amplitude of about $10 \%$ of horizontal scope display. The marker amplitude control affects only the vertical component; therefore, the marker is adjustable from a horizontal position to an angle approaching vertical as the MARKER SIZE control setting is increased.

A rear-panel PROGRAMMING jack provides necessary connections for remote control of frequency, sweep width band selection, and the 0 to 20 dB vernier output level. This jack also provides connections for external amplitude and frequency modulation and external triggering of the sweep rate generator, as well as cornections to internal DC voltages, and sweep and blanking signals.

Selection is accomplished via TTL signals or contact closure.

May be remotely programmed within the selected band by applying a voltage between +10 V and $-10 \mathrm{~V}(-10 \mathrm{~V}$ programs the low frequency end of band).

Tuning sensitivities are:

$$
\begin{array}{ll}
\text { band 1 } & 35.7 \mathrm{mV} / \mathrm{MHz} \\
\text { band 2, 3 } & 17.8 \mathrm{mV} / \mathrm{MHz} \\
\text { band 4 } & 7.1 \mathrm{mV} / \mathrm{MHz}
\end{array}
$$

May be controlled with a remote potentiometer.
May be controlled by setting the front-panel OUTPUT VERNIER for maximum output and applying a DC voltage between 0 and $-4.5 \vee(-4.5 \mathrm{~V}$ programs 20 dB reduction in power). Front-panel METER will indicate the RF output level. Simultaneous AM and level control can be achieved by adding the appropriate DC offset to the modulating signal. See "External AM".

Amplitude modulation can be accomplished according to the specifications below. Simultaneous $A M$ and level control can be achieved by adding the appropriate DC offset to the modulating signal. See "Vernier 0-20 dB Output".

FREQUENCY RANGE
SENSITIVITY

MAXIMUM MODULATION \%

EXTERNAL FM

### 1.2.7 GENERAL

## OPERATING TEMPERATURE

POWER REQUIREMENTS

DIMENSIONS

WEIGHT

### 1.3 OPTIONS

A1

A2

A3

B4

B5

DC to 10 kHz ( 3 dB bandwidth)

1 Vpp per 10\% AM
Varies from $10 \%$ to $90 \%$ depending upon the setting of the OUTPUT VERNIER control as shown in Figure 2-16. Overmodulation will cause the front-panel UNLEVELED light to turn on; however, since the unleveled condition would exist only at the peak or trough of modulation, the light will be less than full intensity.

Any portion of any band not containing a band switching discontinuity point can be swept at any rate up to 10 kHz . $\pm 50 \mathrm{MHz}$ deviation can be obtained at rates up to 50 kHz . Modulation rates up to 200 kHz are possible with reduced deviation and unspecified linearity. Tuning sensitivity is the same as that for remote frequency control.
$0^{\circ}$ to $50^{\circ} \mathrm{C}$

115 or 230 VAC $\pm 10 \%$, 50 to 400 Hz , approximately 25 VA.
30.3 cm wide $\times 13.4 \mathrm{~cm}$ high $\times 34.9 \mathrm{~cm}$ long ( $12^{\prime \prime} \times 51_{1^{\prime \prime}} \times$ $133 / 4^{\prime \prime}$ )
10.5 kg (23 lbs.) net
12.7 kg ( 28 lbs. ) shipping

All options are factory or field installable. A maximum of 5 A1 or A2 options can be installed in the instrument in addition to 1 each of Options A3, B4, and B5.

Single Frequency Marker at any frequency within the instrument range.

Harmonic (comb) Marker at 1, 5, 10, 50, or 100 MHz intervals (other intervals available on special order). Also available is a Dual Harmonic Marker at $0.1 / 1 \mathrm{MHz}$ intervals (occupies two marker sockets).

NOTE: Operating range of $A 2$ options is 1 to 1500 MHz .
Deluxe Harmonic Marker at $1,10,50$, and 100 MHz intervals over entire instrument range.

Pen Lift provides contact closure during forward sweep trace. Binding post terminals are provided on rear panel.

Auxilliary RF Output provides rear-panel RF output signal (approximately -10 dBm , depending on marker options installed) for driving a frequency counter or other similar purpose.

### 1.4 ACCESSORIES

### 1.4.1 FURNISHED WITH INSTRUMENT

INSTRUCTION MANUAL

PROGRAMMING PLUG
1.4.2 AVAILABLE AT EXTRA COST

WIDE BAND RF DETECTORS

RACK MOUNT KIT

SERVICE KIT

Connector and pins provided to mate with jack on instrument rear panel.

Model D153. Frequency range: 1 MHz to 12.4 GHz .

K108 enables instrument to be mounted in a standard 19" wide instrument rack.

K005 provides a module extender, extension cables and adaptor.

### 2.1 INTRODUCTION

This section provides complete installation and operating instructions for the Wavetek Model 2002A. The instructions include information on mechanical installation, electrical installation, front-and-rear-panel features, operating procedures, and programming instructions.

### 2.2 MECHANICAL INSTALLATION

### 2.2.1 INITIAL INSPECTION

After unpacking the instrument, visually inspect external parts for damage to knobs, connectors, surface areas, etc. The shipping container and packing material should be saved in case it is necessary to reship the unit.

### 2.2.2 DAMAGE CLAIMS

If the instrument received has been damaged in transit, notify the carrier and either the nearest Wavetek area representative or the factory in Indiana. Retain the shipping carton and packing material for the carrier's inspection.

The local representative or the factory will immediately arrange for either replacement or repair of your instrument without waiting for damage claim settlements.

### 2.2.3 RACK MOUNTING (K108)

CONTENTS (See Figure 2-1).

| ITEM | QTY | PART NO. |
| :--- | :---: | ---: |
|  |  |  |
| A (Insert) | 2 ea | $1410-00-4650$ |
| B (Side) | 2 ea | $1410-00-5260$ |
| C (Screw) | 8 ea | $2810-17-8108$ |
| D (Screw) | 4 ea | $2810-17-8110$ |

## PROCEDURE

Remove screws from one side panel. Mount items $A$ and $B$ against side panel of the instrument and secure with screws provided. Repeat for other side of unit. If rack mount kit is removed from unit, use screws originally in side panels to avoid possible internal damage.

### 2.3 ELECTRICAL INSTALLATION

### 2.3.1 POWER REQUIREMENTS

This instrument operates from either 115 VAC or 230 VAC supply mains, as selected by the rear-panel AC LINE switch. Before operating this instrument, be sure that the AC LINE FUSE is the correct value for the selected voltage (see Section 2.5).

The Power Supply has been designed to operate over a 50 to 400 Hz line frequency; however, the line operated sweep rate function must be adjusted to the line frequency.

Instruments are shipped from the factory set up to operate at $115 \mathrm{VAC}, 60 \mathrm{~Hz}$ unless otherwise specified.

### 2.3.2 PERFORMANCE CHECKS

The electrical performance of this instrument should be verified prior to actual use. Performance checks for incoming inspection are given in Section 4 of this manual.


Figure 2-1. K108 Rack Mount


Figure 2-2. Front Panel

### 2.4 DESCRIPTION OF FRONT PANEL

Refer to Figure 2-2.
(1) BAND switch selects desired frequency band.
(2) CENTER FREQ/START thumbwheel controls center frequency when MODE switch is set to $\Delta f$ or CW, and start frequency when MODE switch is set to $\mathrm{S} / \mathrm{S}$.
(3) MARKER WIDTH, SIZE controls; outer ring selects marker width (4 positions); inner knob varies marker amplitude.
(4) FREQUENCY SCALE shows center frequency and sweep width, or start/stop frequencies (depending on position of MODE switch). Graduated for all 4 bands.
(5) HARMONIC MARKER switch selects markers generated by the Deluxe Harmonic Marker (Option A3). If this option is not installed, this knob has no function.
(6) SWEEP TIME, VAR/MANUAL controls; outer ring selects sweep time range (4 ranges); line rate, or manual control; inner knob provides manual frequency sweeping with the outer ring set to MANUAL, and vernier control of the sweep time with the outer ring set to any of the 4 sweep time ranges.
(7) SWEEP WIDTH/STOP thumbwheel controls sweep width when MODE switch is set to $\Delta f$, and stop frequency when MODE switch is set to S/S. When the MODE switch is set to CW, this control has no function.
(8) MODE switch selects S/S (Start/Stop), $\Delta f$, or CW mode.
(9) OUTPUT VERNIER, STEP ATTENUATOR; outer ring controls RF output over a 70 dB range $(+10$ to -60 dBm ) in 10 dB steps; inner knob provides vernier control ( +3 to -17 dB ) of RF output.
(10) METER indicates RF output over a 20 dB range (calibrated from +3 to -10 dB ). The METER reading added algebraically to the STEP ATTENUATOR indication is the RF output of the instrument.
(11) UNLEVELED lamp signals when the METER reading is not valid.
(12) RF OUT connector (type N) provides connection for RF output signal.
(13) SLOPE control provides compensation for frequency dependant level variations external to the instrument.
(14) ALC switch closes the internal leveling loop when in the INT position. In the EXT position, an external monitor may be used to control the instrument's RF output (through the ALC IN connector). If the switch is in EXT, and no external monitor is used, the RF output is unleveled and the OUTPUT VERNIER has no effect.
(15) ALC IN connector (type BNC) accepts an external leveling control signal from a remote monitor when the ALC switch is in the EXT position.
(16) BLANKING switch allows the RF output to be blanked during sweep retrace when the switch is in the ON position. When the switch is not on, the RF output is displayed during retrace.
(17) TRIG/RECUR switch selects either recurring sweep of the time selected by the SWEEP TIME control (with MODE switch in $\Delta f$ or $S / S$ ), or triggered sweep, either manually or with an external source (the external trigger input is pin 7 of the rear-panel PROGRAMMING jack). Manual triggering is accomplished by pushing the TRIG/RECUR switch to its full up (momentary) position.
(18) MARKER IN connector (type BNC) accepts an external CW signal to produce a marker at the external frequency on the display.
(19) MARKER switches select which internal markers are active (marker frequency is engraved on pushbutton). The furthest right switch selects internal square wave modulation.
(20) DEMOD IN connector (type BNC) accepts demodulated swept signal from device under test so that markers can be added (the combined signal is available at the VERT OUT connector).
(21) VERT OUT connector (type BNC) provides vertical display signal (demodulated signal plus markers if DEMOD IN is used) for display oscilloscope.
(22) HORIZ OUT connector (type BNC) provides a 0-10 $\checkmark$ triangle wave for driving the display oscilloscope horizontal channel.
(23) MARKER SIZE switch selects large ( $\sim 7 \mathrm{mVpp}$ to $3.5 \mathrm{Vpp})$ markers, small ( $\sim 0.2 \mathrm{mVpp}$ to $\sim 20 \mathrm{mVpp}$ ) markers, or rectified ( $\sim 0.2 \mathrm{mV}$ to 1.25 V ) markers (the marker ampliude is varied by means of the MARKER SIZE control). The rectified markers are designed for use with $X-Y$ recorders.
(24) POWER switch applies AC power to the Power Supply. Pilot light indicates operation.
(25) TILT/NORM switch provides vertical markers in the NORM position, and horizontal markers of fixed amplitude (10\% of horizontal display) in the TILT position when the MARKER SIZE control is set to minimum. Increasing the setting of the MARKER SIZE control will cause the horizontal markers to tilt toward a vertical position. This feature is helpful in identifying frequencies on steep response curves.

### 2.5 DESCRIPTION OF REAR PANEL

Refer to Figure 2-3.
(1) AUX RF OUT connector (type BNC, Option B5) provides approximately -10 dBm RF output.
(2) BLANKING output connector (type BNC) provides pulse for oscilloscope intensity input to remove band stacking transition points from scope display. Switch selects pulse polarity.
(3) SWEEP DWELL switch selects normal or delayed (approximately 4 msec ) sweep.
(4) AC LINE cord provides connection to AC mains via 3 prong plug.
(5) AC LINE switch enables unit to operate from either 115 VAC or 230 VAC supply mains.
(6) AC LINE FUSE is time delay; 1.0 amp for 115 VAC operation, 0.5 amp for 230 VAC operation.
(7) PEN LIFT (Option B4) binding posts provide contact closure during forward sweep when the front- panel SWEEP TIME control is in the $1-10 \mathrm{sec}, 10-100 \mathrm{sec}$, or MANUAL range. In all other ranges, and during retrace, the contacts are open. NOTE: In MANUAL sweep, there is no retrace signal, so the contacts are continually closed.
(8) PROGRAMMING PLUG provides input connections for external trigger, sweep delay, external AM/FM, and remote control of center frequency, sweep width, band selection and RF output. Output connections are provided for sweep ramp, retrace blanking, and Power Supply voltages.

## NOTE

If Options B4, B5 are not installed, blank plug buttons will be installed in the rear panel instead of the indicated connectors.


Figure 2-3. Rear Panel

### 2.6 TYPICAL OPERATING SET-UP

When initally setting up the instrument, first check the rear-panel AC LINE FUSE and switch to be sure the instrument is set for operation with the available AC mains.

Make connections between the instrument, the device under test, and the oscilloscope as shown in Figure 2-4. Since hum, RF leakage, and spurious signal pick-up must be kept to a minimum, it is essential that good connections and grounds be maintained throughout the entire set-up. Use coaxial cables with BNC connectors wherever possible. The RF output cable is especially critical. It should have a characteristic impedance of 50 ohms, and should be kept as short as practical (under 3 feet). If the input impedance of the device under test is not 50 ohms, a matching network, as shown in Figure 2-4, should be used to ensure a constant amplitude input signal to the device under test.

After the RF signal passes through the RF circuit of the device under test, it must be demodulated before being connected to the DEMOD $\operatorname{IN}$ of the instrument. If a demodulator is not a part of the device under test, one must be added externally (see Figure 2-4). The input impedance of the demodulator must present the proper load to the RF circuit being tested. The Wavetek Model D153 RF Detector is recommended for 50 ohm applications.

Turn the front-panel POWER switch on. The pilot light should indicate an operating condition.

## NOTE

This instrument does not require a warmup period unless it is to be used at the extreme limits of its specifications.

After completing the set-up, adjust the instrument frontpanel controls for the required center frequency, sweep width, output amplitude, and sweep rate. Turn the desired markers on and adjust their size and width.

### 2.7 SPECIAL OPERATING NOTES

### 2.7.1 ERRORS FROM SWEEP RATE EFFECTS

When sweeping RF circuits having rapid amplitude changes, errors may occur, due mainly to detector delays. Decreasing the detector output time constant will minimize this effect. Figure 2-5 illustrates sweep rate effect.

To check for sweep rate effect, first set the sweep width to its lowest practical setting, then reduce sweep time while closely observing the swept output response. Any change in the response indicates the sweep rate is too fast for a true response. When a further reduction of sweep time
does not change the response, a true response has been obtained.

### 2.7.2 EFFECTS FROM OVERLOADING

The use of excessive signal from the instrument can overload the receiver circuits. To assure that this condition is not present, and that the response is a true representation of the device under test, turn the OUTPUT STEP and VERNIER controls to minimum output amplitude. Gradually increase the output amplitude until a response is obtained. Further increasing the output amplitude should not change the configuration of the response envelope does change, such as flattening at the top, decrease the output just far enough to restore the proper configuration.

### 2.7.3 MAKING MEASUREMENTS AT LOW LEVEL

When making measurements at low levels, radiation and ground loops become problems. Using double shielded cables for cables carrying RF signals helps minimize the radiation problem. Ground loops causing hum pick-up can sometimes be eliminated by completing only one ground connection between each instrument. This applies particularly to the scope horizontal input. If the ground connection is made at the vertical input terminial, an additional ground at the horizontal input terminal will often result in hum pick-up.

### 2.7.4 SWEEP DWELL

In order to stabilize external circuits (such as when using a network analyzer), it is sometimes desirable to turn the RF signal on prior to the start of the sweep. This can be accomplished using the rear-panel SWEEP DWELL switch. When the switch is turned on, the RF output is tuned on approximately 4 msec before the sweep begins.

## NOTE

This applies only to the four variable time positions of the SWEEP TIME control, and does not apply to either the LINE or MANUAL position.

### 2.7.5 OPERATION WITH X-Y PLOTTERS

Two features are incorporated into the instrument to facilitate operation with X - Y plotters.

First, a marker clamp switch (part of the front-panel MARKER SIZE switch) which converts the high frequency marker signals to lower frequencies, compatible with the operating speed of the marker pen.

The second feature (Pen Lift) is available as Option B4, and is described in Section 2.8.4.

MODEL 2002A


Figure 2-4. Typical Test Set-up


Figure 2-5. Sweep Rate Effects


Figure 2-6. External Monitor Output Signal

### 2.7.6 OPERATION WITH EXTERNAL MONITOR

Operation with an external monitor can produce a flatter (less amplitude variation) input signal to the device under test than is obtainable with the internal monitor, since the monitor point is located at the point where greatest flatness is desired and is not affected by cable VSWR or input impedance of the device under test. Another application is to level at the output point of a wide band power amplifier in. order to increase the output power capability of the sweep generator.

To operate with an external monitor, first set the OUTPUT STEP and VERNIER controls for maximum ( +13 dBm ). Next, connect the output from the external monitor to the front-panel ALC IN connector and set the ALC switch to the EXT poisition. The signal from the external monitor must be of negative polarity between 0.2 and 2 volts. If the signal is larger than 2 volts, use a resitive divider to obtain the less-than-2 volts signal. While observing the output from the monitor on an oscilloscope, adjust the OUTPUT VERNIER until the monitor signal becomes leveled (refer to Figure 2-6).

## NOTE

If the requirement of a 0.2 to 2 V monitor signal results in overloading of the device under test, insert an external attenuator pad between the monitor and the device under test.

### 2.7.7 SLOPE

Up to $\pm 1 \mathrm{~dB} / \mathrm{GHz}$ amplitude slope may be introduced to compensate for frequency-dependant variables in the test system external to the instrument. The pivot point for the slope is 1 MHz , with the maximum amplitude change due to slope introduction being $\pm 2.5 \mathrm{~dB}$ at 2500 MHz (refer to Figure 2-7).

When the front-panel SLOPE control is set to its mid-position adjustment ( 0 slope), an uncorrected signal will be displayed.

### 2.7.8 1 KHz MODULATION

This feature provides 1 kHz square wave modulation of the RF output signal. On/off control is provided by a push button switch on the instrument's front panel. The 1 kHz modulating frequency may be adjusted using the control located on top of module M121 (see Figure 5-22).

### 2.7.9 PEN LIFT (OPTION B4)

This option provides a contact closure during forward sweep time. During retrace, the contacts are open. This option can be used to operate the pen lift of an $X-Y$ plotter. It is active only during the two slowest settings of the SWEEP TIME switch ( 1 to 10 seconds and 10 to 100 seconds) and during manual sweep. (During manual sweep the contacts are always closed.) The connections for Option B4 are two binding posts on the instrument rear panel.

### 2.7.10 AUX RF OUT (OPTION B5)

This option provides an RF signal at approximately - 10 dBm through a rear-panel connector. This signal is identical in frequency and sweep characteristics to the signal from the front-panel RF OUT connector; however, there is no provision for controlling the level of the auxilliary signal. (The actual output level of the auxilliary signal is dependent on the number of marker options (A1, A2, A3) installed in the instrument. The more marker options, the lower the output level.) Likewise, the auxilliary signal will show FM, but will not show AM.

## NOTE

For proper marker operation, the AUX RF OUT connector must be either connected to a $\mathbf{5 0} \mathbf{~ o h m}$ device, or terminated in 50 ohms (terminator provided).

### 2.8 PROGRAMMING

### 2.8.1 INTRODUCTION

Connections for remote control of output level, center frequency, sweep width, band selection, and sweep triggering, and also external AM and FM are provided in the rear-panel PROGRAMMING jack. The jack and its pin functions are detailed below (refer to Figure 2-8).

### 2.8.2 OUTPUT PINS

The first group of pins are voltage and signal outputs. Pin 1 is a common ground. Pins 2 and 3 provide $\pm 10 \mathrm{~V}$, used for remote frequency tuning. Pins 4 and 5 are the $\pm 18 \mathrm{~V}$ main regulated supplies, and can be used in external applications which draw less than 50 mA each.

Pin 8 is the sweep ramp with varies over a $\pm 10 \mathrm{~V}$ range. This signal is similar to the signal from the front-panel HORIZ OUT connector, except that the latter ranges from 0 V to +10 V . These ramps are independent of frequency and sweep width.


Figure 2-7. Slope

|  |  |  | PIN | FUNCTION | PIN | FUNCTION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 33 | $\bigcirc \bigcirc \bigcirc$ | 36 | I Outputs |  | III Unused |  |
|  |  |  | 1 | Ground | 13,1 | 27-36 Unused |
| 29 | $\bigcirc \bigcirc \bigcirc$ | 32 | 2 | +10 V | IV Inputs |  |
|  |  |  | 3 | -10 V | 6 | Output Leve1/AM |
| 25 | $\bigcirc \bigcirc$ | 28 | 4 | -18 V | 7 | Ext Trigger |
|  |  |  | 5 | +18 V | 10 | Cent Freq |
| 21 | 00 | 24 | 8 | Sweep Ramp | 12 | SW/FM/ / Lock |
|  |  |  | 14 | Ret Blanking | 21 | Band 2B |
| 17 | 000 | 20 | 25 | Sync | 22 | Band 2A |
|  |  |  | 26 | $1 \mathrm{~V} / \mathrm{GHz}$ Ref | 23 | Band 3 |
| 13 | $0 \bigcirc$ | 16 |  | orma1 | 24 | Band 4 |
|  |  |  |  | 0 Cent Freq |  |  |
| 9 | 00 | 12 | 11 | 2 Sweep Width |  |  |
|  |  |  | 15 | 6 Start/Stop |  |  |
| 5 | $\cdots 0$ | 8 | 18 | 9 Band Select |  |  |
| 1 |  | 4 | Pin | is internal | poin | Do not use ext |

Figure 2-8. PROGRAMMING Plug Pin Configuration

Pin 14 provides a retrace blanking signal for a display oscilloscope. The levels at this connector are +16 V ( RF off) and -16 V (RF on).

Pin 25 provides a TTL "high" signal whenever the RF output frequency crosses a band switching discontinuity point ( $500,1000,1500 \mathrm{MHz}$ ). At all other times, the output is TTL "low". This signal finds use in working with network analyzers.

Pin 26 is a $1 \mathrm{~V} / \mathrm{GHz}$ reference which provides an indication of the instantaneous RF output frequency. If the RF output frequency is 1200 MHz , pin 26 will be +1.2 V . If the RF output is swept from 1600 to 2400 MHz , the voltage at pin 26 will follow the frequency, producing a +1.6 V to +2.4 V ramp.

### 2.8.3 NORMAL OPERATION PINS

The second group of pins is used to provide normal frontpanel operation of the instrument. Pin 9 is jumpered to pin 10, pin 11 is jumpered to pin 12 , pin 15 is jumpered to pin 16, and pin 18 is jumpered to pin 19. A plug containing these jumpers must be installed on the rear-panel PROGRAMMING jack in order to accomplish normal operation.

### 2.8.4 UNUSED PINS

The third group of pins is unused.

### 2.8.5 INPUT PINS

The functions of the last group of pins are as follows:

## REMOTE FREQUENCY CONTROL (PIN 10)

Normal front-panel control of center frequency is provided by a jumper wire between pins 9 and 10 of the rear-panel PROGRAMMING plug. To remotely control the center frequency, remove the jumper and connect pin 10 to the external control, as shown in Figure 2-9.

## REMOTE SWEEP WIDTH CONTROL (PIN 12)

Normal control of sweep width is provided by a jumper between pins 11 and 12 of the rear-panel PROGRAMNING plug. To remotely control the sweep width, remove the jumper and connect pin 12 to the external control, as shown in Figure 2-10.

## NOTE

When using the instrument with remote control of sweep width, external FM, or in phase lock operation, the frontpanel MODE switch must be set to $\Delta \mathrm{f}$.

EXTERNAL FM (PIN 12)
For FM, remove the pin 11 to 12 jumper and connect the modulating source as shown in Figure 2-11.

The FM signal should have an average potential of 0 V . Frequency sensitivity is $35.7 \mathrm{mV} / \mathrm{MHz}$ for band $1,17.8$ $\mathrm{mV} / \mathrm{MHz}$ for bands 2 and 3 , and $7.1 \mathrm{mV} / \mathrm{MHz}$ for band 4 . Maximum frequency deviation as a function of modulating frequency is shown in Figure 2-12.

The peak amplitude of the modulating signal plus the DC voltage applied to pin 10 of the PROGRAMMING jack should not exceed $\pm 10 \mathrm{~V}$, since a greater voltage would cause the instrument to sweep beyond its band limits.

## PHASE LOCK (PIN 12)

When the instrument is operated in a closed-loop synchronizing system, the correction voltage is applied to pin 12 of the PROGRAMMING jack. Again, the MODE switch must be set to $\Delta \mathrm{f}$ and the pin 11 to 12 jumper must be removed (refer to Figure 2-13).

## REMOTE OUTPUT LEVEL (PIN 6)

For remote control of the 0 to 20 dB OUTPUT VERNIER control range, first adjust the front-panel OUTPUT VERNIER control fully clockwise. This will produce a METER reading of 3. Connect the external level control as shown in Figure 2-14. The program level will be indicated on the front-panel METER.

EXTERNAL AM (PIN 6)

To produce $A M$, connect the modulating source to pin 6, as shown in Figure 2-15.

The modulating frequency may vary over a 0 to 10 kHz (at 3 dB point) range. The modulation sensitivity is $1 \mathrm{Vpp} /$ $10 \%$ modulation. The maximum \% AM is dependent upon the front-panel OUTPUT VERNIER setting, as shown in Figure 2-16.

## EXTERNAL TRIGGER (PIN 7)

The Sweep Time circuit may be remotely triggered by applying a +10 V pulse to pin 7 of the rear-panel PROGRAMMING plug. For proper operation, the frontpanel SWEEP TIME control must be set to one of the four variable time positions, and not to MANUAL or LINE. The TRIG/RECUR switch must be set to TRIG. The repetition rate of the external tirgger should be slower than the frequency repetition rate set by the front-panel SWEEP TIME and VAR/MANUAL controls.


Figure 2-12. Maximum FM Deviation

## REMOTE BAND SELECTION (PINS 21-24)

For remote control of band selection, remove the jumper between pins 18 and 19 on the PROGRAMMING plug. Any frequency band may now be selected by applying a ground (contact closure or TTL) signal to pin 21, 23, or 24 on the PROGRAMMING plug. Applying a ground signal to pins 21 and 22 simultaneously will select the second half of band 2 ( $1000-1500 \mathrm{MHz}$ ) (see Section 3.13). If no ground signal is applied, band 1 will be selected.


Figure 2-15. External AM


Figure 2-16. Maximum \% AM

### 3.1 INTRODUCTION

This section first presents an overall block diagram view of the Model 2002A, followed by a more detailed description of each module and assembly.

Before beginning the actual circuit descriptions, it would be well to become familiar with the mechanical arrangement of the instrument. This will enable the block diagram and circuit descriptions to be associated with the physical locations in the instrument, providing a better overall understanding of the instrument (refer to Figure 5-22).

### 3.2 BLOCK DIAGRAM

The block diagram in Figure 3-1 contains both block and module information. The blocks contained within each module are indicated by the module outline.

The general operation of the Model 2002A is as follows:
The front-panel CENT FREQ and SWEEP WIDTH control settings are fed into the M102A and M103A Sweep Drive modules, where they are combined into a single signal. This signal (sweep drive) is used to drive the varactor diodes in the appropriate Sweep Oscillator (M109 or M110). Necessary level shifting, shaping, and amplitude control are accomplished in the Sweep Drive modules.

The Sweep Oscillator output is fed into the MA111 Wide Band Amplifier, and then through the Step Attenuator to the RF output. Leveling is accomplished by a monitor diode in the MA111 which compares the output level to a reference voltage supplied by the OUTPUT VERNIER. Any error is amplified in the M104A Leveler module, and correction is made at the PIN diode leveler in the MA111.

The marker circuit is composed of the M105 Marker Adder module, the M6C External Marker module, and the various marker options selected by the customer. The marker circuit uses a sample of the RF signal (sweep sample) which is also leveled in the M104A Leveler. This leveling not only provides a constant-amplitude sweep sample signal to the marker circuit, but also standardizes the sweep sample signals in all instruments, assuring proper operation of field installed marker options.

More detailed descriptions of the individual modules and assemblies are provided below. Schematics are in Section 7.

### 3.3 DPS2A - POWER SUPPLY

The Power Supply provides DC power for the rest of the instrument, and a 27 VAC signal to the M101B Sweep Rate Generator module.

The transformer steps the line voltage down to 27 VAC, a level which can be used by the DC-producing circuits. (A portion of this 27 VAC signal is sent to the M101B for use in the line rate sweep function of the instrument.) Fullwave rectifiers and filter capacitors convert the AC signal to DC.

A portion of this 27 VDC signal is sent to the +20 V regulator mounted on the instrument chassis, the rest is sent to the $\pm 18 \mathrm{~V}$ and +7 V supply circuits.

The $+18 \vee$ circuit has a temperature-compensated precision voltage reference. This reference is compared to the output voltage by an error amplifier which corrects any error in the output voltage.

The -18 V circuit compares the +18 V and -18 V outputs and holds the difference in their magnitudes to zero.

The +7.3 V circuit uses a three-terminal adjustable voltage regulator IC to provide a pre-regulated +7.3 V output. This voltage supplies other voltage regulators throughout the instrument.

### 3.4 M101B - SWEEP RATE

## INTRODUCTION

This module generates the basic sweep ramp for the instrument, an inverted ramp used in S/S mode, and a synchronous square wave used for blanking.

The M101B is basically a hysteresis oscillator, consisting of a hysteresis switch (IC5A) and an inverting integrator (IC1 with C9). The sweep ramp is the integrator output, while the inverted ramp (derived from the sweep ramp) is the output of an inverting buffer (IC2).

## SWEEP RAMP

Diodes CR17 and CR18 clip the hysteresis switch output to produce a $\sim \pm 10.6 \mathrm{~V}$ square wave. CR13 and CR14 reduce the level to $\sim \pm 10 \mathrm{~V}$, and also provide temperature compensation. The $\pm 10 \mathrm{~V}$ square wave is positively fed back to the non-inverting input of the hysteresis switch along with delayed negative feedback from the integrator.

When the negative feedback outweighs the positive feedback, the non-inverting input crosses the ground reference on the inverting input and the switch changes state. This occurs when the hysteresis switch output and the sweep ramp are equal in magnitude but opposite in polarity. The switch output is buffered by IC6B and sent through the sweep time resistor network to pin 10 of the module, the inverting integrator input.

## SWEEP TIME

Sweep time is the time required for the sweep ramp to rise from -10 V to +10 V , and is determined by the current fed into the inverting integrator input. Sweep time is selected by the front-panel SWEEP TIME control, and is calibrated by the Freq. Adj. control (R60).

## TRIGGERED SWEEP

For operation in recurring sweep mode, +18 V is applied to pin 2 of the module. For triggered sweep mode, this voltage is removed, shutting off Q 2 and removing the reverse bias on CR12. This lowers the hysteresis switch trip point to -10.7 V and arms the clamping circuit (IC3A, Q1, and associated components). As the descending ramp reaches -10 V , Q 1 fires and clamps the ramp at -10 V . Since the ramp cannot reach -10.7 V , recurring sweep is prevented.

The trigger circuit (IC3B and associated components) is armed when clamping has occurred. The positive trigger pulse is applied (either from the front-panel switch or the rear-panel PROGRAMMING plug) to module pin 5, and is fed through C11 to IC3B pin 5. This switches IC3B pin 7 to +18 V . As pin 5 drops back below the slightly positive voltage on pin 6 , pin 7 switches to -18 V , sending a negative pulse to the hysteresis switch, causing it to switch states and trigger the sweep.

## LINE RATE SWEEP

Line rate sweep is an automatically triggered mode, the trigger source being a 27 VAC signal from the Power Supply. Pin 9 of the module is the line rate enable. When a +18 V signal is present, the reverse bias on CR10 is removed, and the 27 VAC is sent to IC3B as the trigger signal.

## SWEEP DWELL

A sweep dwell feature is also provided for use with network analyzers. The dwell is similar to the clamp described above, but differs in that it is produced at the start of the forward trace (hysteresis switch negative, RF output available), while the clamp occurs at the end of the retrace (hysteresis switch positive, RF output blanked). When a positive voltage is applied to pin 15 of the module, the bias on pin 6 of IC5B is made less negative. When the hysteresis switch output goes negative, a large negative spike is sent to IC5B pin 5, turning off Q3. The RF blanking is removed at this time by IC6A. With Q3 turned off, module pin 12 is pulled to ground, shutting off the inverting integrator. As pin 5 of IC5B returns to ground potential, it crosses the reference still on pin 6 , thus turning on Q 3 and starting the integrator.

## MANUAL SWEEP

During manual sweep, +18 V is applied to pin 1 of the module, which places $\sim 2.5 \mathrm{~V}$ bias on pin 2 of the hysteresis switch and locks the switch negative. CR1 and CR3 are forward biased, so that IC1 is now a linear amplifier instead of an integrator. Manual Limit control R20 is adjusted such that the front-panel VAR/MANUAL control varies the output of IC1 between -10 V and +10 V ; thus, the ramp can be manually swept by means of the VAR/ MANUAL control.

### 3.5 M102A - SWEEP DRIVE

This module provides the correct sweep drive voltage required by sweep oscillators 1 and 3 .

The M102A sums the voltage from the CENT FREQ control with a portion of the sweep ramp selected by the SWEEP WIDTH control setting. The combined ramp is then shaped into the proper signal to drive the oscillators. The unshaped ramp and two offset ( $\sim \pm 7.5 \mathrm{~V}$ ) ramps appear as outputs from the M102A to the M103A, where they are used in shaping the sweep drive signals for oscillators $2 A$ and 2B.

The shaping of the sweep drive signals is accomplished by adding the two offset ramps to the combined ramp via 2.2 kohm resistor networks. As the ramp rises and falls, diodes strung along the networks are successively forward biased at ~2 V intervals. As a result, the current to the input of the sweep drive IC is changed as each diode becomes forward biased, thus changing the effective input impedance to the IC, and so changing its gain. An increase in gain will cause an expansion of the sweep oscillator range.

Some of the diodes also feed current to an inverting amplifier, which, in turn, feeds its output to the sweep drive IC.

The effect of this inversion is to subtract current from the sweep drive IC, thus decreasing its gain and compressing the sweep oscillator range.

The actual amount of gain at each interval is determined by a potentiometer (Lin control) in series with each of the diodes. In this way, the sweep drive is shaped to produce a linearly swept RF output signal.

### 3.6 M103A - SWEEP DRIVE

This module supplies the centering voltages to the four voltage-controlled sweep oscillators in the instrument, and also provides the correct sweep drive voltages required for oscillators 2 A and 2 B .

The centering voltages are adjusted with potentiometers R7, R8, R9, and R10. These voltages are applied as bias voltages to the varactor diodes in each sweep oscillator. The bias is adjusted such that each sweep oscillator will be at its center frequency when its sweep drive voltage is zero.

The sweep drive circuitry in the M103A is very similar to that in the M102A described above. The combined and offset ramps from the M102A are added in 2.2 kohm resistor networks, turning on the shaping diodes in succession and effectively changing the input impedance and gain of the sweep drive IC's. Instead of an inverting amplifier, however, some of the diodes feed the noninverting input of the sweep drive IC's, causing compression of the sweep oscillator range. The other diodes feed the inverting input of the sweep drive IC's, causing the sweep oscillator range to expand. As in the M102A, the Lin controls determine the amount of compression or expansion, and so enable a linearly swept RF output signal to be produced.

### 3.7 M104A - LEVELER

## INTRODUCTION

This module contains the leveling circuitry for both the instrument RF output and internal sweep sample, and also drives the front-panel METER and UNLEVELED lamp.

## SWEEP SAMPLE LEVELING

To level the sweep sample, a reference voltage is set on pin 6 of IC2B via level control R2. Pin 5 is the input from the MA111 sweep sample monitor diode. The output from the IC is used to drive a pair of PIN diode attenuators in the MA111, thus leveling the sweep sample.

## RF OUTPUT LEVELING

The OUTPUT VERNIER voltage is buffered by IC1B. The

Level Max control (R12) calibrates the leveler when the VERNIER is fully cw. The output from this control is fed through a temperature compensation diode in the MA111 back to the M104A to be used as part of the RF leveler reference. The Level Min control (R23) calibrates the leveler when the VERNIER is fully ccw.

IC3 is the RF leveler. The composite voltage from R23 and R12 is used as a reference on pin 2. The output from the MA111 RF output monitor diode is applied to pin 3. The IC output, buffered by Q6, drives a PIN diode attenuator in the MA111, thus leveling the RF output.

## METER DRIVE

The OUTPUT VERNIER signal is buffered by IC2A, and is used to drive the output METER. The METER reading is calibrated with the Meter Cal control, R18.

## UNLEVELED LAMP DRIVE

Q2, Q3, and Q4 form a window detector, and turn on the front-panel UNLEVELED lamp when the leveler output exceeds its normal range.

### 3.8 M105 - MARKER ADDER

The function of this module is to take the small beatfrequency marker signals from the various marker options, amplify them, and send them to the front-panel MARKER SIZE control to be added to the demodulated RF signal for display.

Two parallel amplifiers are used in this module. The output of one of the amplifiers is adjusted with the Size Ratio control, R29, to produce markers of different sizes.

Transistors Q 1 through Q 5 are low-noise preamplifiers. Q9, Q10, Q12, Q13, Q22, and Q23 are controlled by the front-panel MARKER WIDTH switch. When selected, these FETs switch in capacitors to limit the frequency response of the amplifiers, thus producing narrow markers. With the MARKER WIDTH switch in either of its two narrowest settings, Q6 and Q8 are activated, switching in C29 and C8 on the emitters of the preamplifiers, thus increasing the low frequency gain and producing a narrowed center frequency null for the narrowed marker. IC1 and IC2, along with output transistors Q14, Q15, Q16, and Q17, produce the high gain needed for the marker output.

### 3.9 M109 - SWEEP OSCILLATOR 1

This module generates the $1-530 \mathrm{MHz}$ band 1 (plus oversweep) frequency by heterodyning the output of an 1198 MHz fixed oscillator (Q5) and an 1199-1728 VCO (O2). The VCO is biased to oscillate at 1448 MHz when the sweep drive signal is 0 V , and varies above and below this
frequency as the sweep drive is varied.) Both outputs are buffered and leveled before being heterodyned in the mixer (CR101 through CR104). The mixer IF output is preamplified (O201 through Q204) and sent through the M110 to the MA111 Output Amplifier.

During blanking, Q4 turns on, turning off Q202 and Q203, thus eliminating the RF output signal.

Both oscillators are turned on by a -18 V signal from the M131 Band Select module. This signal also turns on IC2 which activates the sweep filter (CR202 and L205). This filter is controlled by the same sweep drive signal which controls the VCO, and serves to reduce the harmonic content of the preamplified output.

In CW mode, the sweep drive signal becomes a DC voltage, and -18 V is applied to pin 16 of the module, turning on Q1. This switches C 6 to ground, thus reducing noise on the sweep drive signal and lowering the residual FM of the RF output signal.

### 3.10 M110 - SWEEP OSCILLATORS 2A, 2B, AND 3

This module generates the 500 to 2500 MHz output frequencies. The M110 consists mainly of three separate VCOs. The VCOs are turned on individually by -18 V signals from the M131 Band Select module. Each VCO is biased to oscillate at its respective band center frequency when its sweep drive signal is 0 V . As the sweep drive signal varies, so does the frequency of the selected VCO. A PIN diode switch at the output of each VCO couples the output signal to the module output, J 2 , and also serves to isolate the VCO from the other two VCOs. From J2, the output signal is sent to the MA111 Output Amplifier.

When band 1 is selected, the B-1 signal turns on the PIN diode switch formed by CR8 and CR9, routing the M109 output through to J2.

During CW operation, the sweep drive signals are DC voltages. FET switches $\mathrm{Q} 3, \mathrm{Q} 4$, and Q 6 are activated, switching capacitors C32, C35, and C47 to ground. This reduces the noise on the sweep drive signals, and so reduces the instrument's residual FM.

In oscillators 2A and 2B, RF blanking is accomplished by turning the VCO off. Oscillator 3, having a slower on/off response, is left on during blanking, and the output is turned off via the PIN diode switch formed by CR18, CR19, CR24, and CR25.

### 3.11 MA111 - OUTPUT AMPLIFIER

The MA111 is a six-stage amplifier arranged in two sections of three stages each, the output of each section being individually monitored and leveled. The output of the first
section feeds the input to the second section, and also supplies a sweep sample output to the marker modules.

The collector voltage and the base current of each transistor stage is individually adjusted at the factory by potentiometers on the bases of the transistors (Q301 to O312). These pots are carefully trimmed for optimum gain and distortion, and should be readjusted only by qualified personnel.

Field checks on this assembly should be limited to checking for the proper RF input, and for the proper signals from the +20 V Power Supply and the M104 Leveler module. If these tests show the Amplifier itself to be defective, the unit should be returned to the factory for servicing.

Also included in this assembly are the sweep sample monitor diode, the output monitor diode, and the PIN diode leveler attenuators. The operation of these is discussed in connection with the M104A Leveler module.

### 3.12 M121 - MODULATOR

This module performs four basic functions. It provides the 1 kHz square wave modulation for low-level recovery applications, the oscilloscope horizontal drive signal, the slope signal, and applies the AM signal from an external source to the OUTPUT VERNIER.

## SQUARE WAVE MODULATION

IC3 and its associated components form a 1 kHz square wave oscillator, the output of which $(\sim 0$ to $+16 \mathrm{~V})$ is used to blank the RF output at a 1 kHz rate. The oscillator is active only when +18 V is applied to module pin 1 via the front-panel 1 kHz MOD pushbutton.

## SCOPE HORIZONTAL

Resistors R7 and R8 sum the sweep ramp from the M101B Sweep Rate module with a +10 V reference to produce the 0 to +10 V horizontal output signal. This signal is available at the SCOPE HORIZ OUT connector, and is used to drive the horizontal input of an oscilloscope.

## SLOPE

IC1B amplifies the $1 \mathrm{~V} / \mathrm{GHz}$ ramp from module pin 9 . The amplified ramp is applied to IC1A and IC2. R9 adjusts the gain of IC1A and nulls any internally-produced slope, while the gain of IC2 is controlled by the front-panel SLOPE control. IC4A sums the outputs of IC1B and IC2 and applies the combined signal to the OUTPUT VERNIER. IC4B provides a correction voltage to the Int Slope Null control (mechanically connected to the OUTPUT VERNIER), and thus to the front-panel METER.

## ANIPLITUDE MODULATION

The external AM signal from the rear-panel PROGRAMMING jack is buffered by IC4A and applied to the OUTPUT VERNIER, thus modulating the instrument RF output.

### 3.13 M131 - BAND SELECT

This module takes the programming information from the M132 Interface module and provides the signal used to enable each oscillator at the proper time. The M131 also provides the frequency/sweep program for the Sweep Drive modules, the $1 \mathrm{~V} / \mathrm{GHz}$ reference signal, and the band switch pulse for the M101B and M132.

## BAND SELECTION

The M131 takes the B2+, B2B+, and B4+ signals from the M132, and the band 3 signal directly from the BAND switch (or PROGRAMMING jack), and converts them to the B-1, B-2A, B-2B, and B-3 oscillator enable signals. IC3A, IC3B, and IC4A are comparators which perform this conversion. IC4B prevents the shifting of the crossover points when the sweep time is changed.

The easiest way to see how the band selection takes place is to examine the selection process for each of the BAND switch (or PROGRAMMING jack) settings.

Band 1: The sweep program (all or part of the -10 V to +10 V sweep ramp from the SWEEP WIDTH/STOP control) is inverted by IC1A. R59 and R66 set a reference of $\sim-13 \mathrm{~V}$ at pin 3 of IC3A. Since the inverted sweep ramp applied to pin 2 of IC3A is always more positive than the -13 V reference, comparator IC3A puts out -18 V at all times. This -18 V turns on Q 10 , which turns on Q 14 , which causes the $-18 \vee \mathrm{~B}-1$ signal to be put out at module pin 5 . The -18 V at IC3A pin 1 also causes comparators IC3B and IC4A (through CR48 and CR39) to put out +18 V , thus keeping the $\mathrm{B}-2 \mathrm{~A}, \mathrm{~B}-2 \mathrm{~B}$, and $\mathrm{B}-3$ signals at +18 V and the oscillators turned off.

## NOTE

In the absence of a +18 V B2+, B4+, or ground band 3 signal, the M131 will default to band 1 programming.

Band 2 (front panel): The $+18 \vee \mathrm{~B} 2+$ signal turns on Q 9 through CR32, thus turning on Q 7 and Q 8 which puts $\sim+18 \mathrm{~V}$ at the cathode of CR38. This removes the -18 V at this point and allows $R 69$ to set the reference at pin 5 of IC3B at 0 V . The inverted sweep ramp is applied to IC3B pin 6. During the positive portion of the ramp, IC3B puts out -18 V at pin 7, turning on Q 11 and Q 15 , to put out the -18 V B-2A signal at module pin 16.

During the negative portion of the inverted ramp, the output of IC3B goes positive. The -18 V signal from IC3B pin 7 through CR40 which had held IC4A pin 2 negative is removed, and IC4A pin 2 goes positive due to +18 V through CR36. Pin 1 of IC4A goes negative, turning on Q12 and Q 16 , thus turning on the $-18 \mathrm{~V} \mathrm{~B}-2 \mathrm{~B}$ signal at module pin 15.

The output of IC3A is held positive by +18 V applied to pin 3 through CR31 and CR33. The emitters of Q7 and Q9 are held at near-ground potential since module pin 10 is grounded through an external diode (CR3 on the BAND switch), but Q 8 is also turned on, preventing Q 6 from turning on.

Band 2 (PROGRAMMING jack): The +18 V B2+ signal will turn on only band 2A ( $500-1000 \mathrm{MHz}$ ). If band 2B ( $1000-1500 \mathrm{MHz}$ ) is desired, both the band 2 and band 2B PROGRAMMING jack pins ( 22 and 21) must be grounded to provide the $\mathrm{B} 2+$ and $\mathrm{B} 2 \mathrm{~B}+$ signals to the M131. If both bands $2 A$ and $2 B$ are desired, a sensing circuit must be used to detect when the sweep ramp (PROGRAMMING jack pin 8) crosses 0 V . The sensing circuit could then supply (or remove) ground to PROGRAMMING jack pin 22 for band 2B operation.

For band 2 A , the +18 V B2+ signal sends the output of IC3B negative as in front-panel operation; however, the reference on pin 5 of IC3B is not 0 V , but a negative voltage. This is true because module pin 10 is not grounded, but floating. Thus, Q 9 and Q 8 are not turned on. The result is that band 2A is continuously enabled, and even if the voltage at pin 6 of IC3B goes below 0 V , the comparator output remains negative, the $\mathrm{B}-2 \mathrm{~A}$ signal remains -18 V , and the band 2A oscillator tries to sweep above its limit (above 1000 MHz ). (This oscillator will sweep slightly above 1000 MHz , allowing operation in the vicinity of 1000 MHz without band switching.)

For band 2 B , both the $+18 \vee \mathrm{~B} 2+$ and $\mathrm{B} 2 \mathrm{~B}+$ signals are active. The $\mathrm{B} 2 \mathrm{~B}+$ places +18 V on pin 5 of IC3B, keeping band 2A disabled and enabling band 2B. The B2+ signal holds the outputs of the other comparators positive as in front-panel operation. The result is that band 2 B is continuously enabled, and if the voltage at pin 2 of IC4A goes above 0 V , the band 2B oscillator will try to sweep below its range (below 1000 MHz ). (This oscillator will sweep slightly below 1000 MHz , allowing operation in the vicinity of 1000 MHz without band switching.)

Band 3: The band 3 ground signal turns on $Q 7$ which allows Q 6 to turn on. This applies $\sim+18 \mathrm{~V}$ to IC3A pin 3, IC3B pin 5, and IC4A pin 3 through CR26, CR35, and CR37. The outputs of IC3A, IC3B, and IC4A are all +18 V , keeping Q10, Q11, and Q12 turned off and their collectors open. This allows Q13 to turn on, which turns on Q17 and thus the $-18 \vee \mathrm{~B}-3$ signal at module pin 14.

Band 4: The +18 V B4+ signal causes the comparator references to be set by R57, R60, and R63. This causes the comparators to change states as the inverted sweep ramp (applied to the inverting inputs) passes through the reference voltage levels. Thus, the oscillator enable signals are turned on sequentially as the sweep progresses.

## FREQUENCY/SWEEP PROGRAM

This circuit takes the sweep ramp from the M101B and divides it into as many ramps as there are oscillators to be used. The frequency program, sweep ramp, and offset program are summed at the input of amplifier IC'1B. The output of the amplifier is the combined frequency/sweep program for the Sweep Drive modules.

During each cycle of the sweep ramp, diodes CR1 through CR3 conduct as selected by the incoming B2+, B4+, and band 3 signals. As each set of diodes conducts, FET switches Q1, Q2, and Q3 switch in resistor sets to change the gain of amplifier IC1B. The -18 V B-1, B-2A, B-2B, and $B-3$ signals also cause one of the diodes (CR15 through CR18) at the input of IC1B to conduct, switching in a pre-set (via R39 through R46) offset current. In this way, a separate frequency/sweep program can be provided for each oscillator. This is important since each oscillator requires a -10 V to +10 V ramp to program it to sweep its full range (a partial ramp programs only a portion of the range). The offset currents and switched amplifier gain produce the proper frequency/sweep program output for each oscillator as it is enabled.

When band 3 is enabled, FET switch Q3 is off, meaning R13 is in the feedback path of amplifier IC1A. This doubles the integrating time constant of the amplifier, and so
doubles the sweep time of the frequency sweep program for band 3 . This is necessary since oscillator 3 sweeps twice the range of oscillators $1,2 A$, and $2 B$, and doubling the sweep time ensures a constant frequency vs. time relationship.

## $1 \mathrm{~V} / \mathrm{GHz}$ REFERENCE

The inverted sweep ramp from IC1A is fed into amplifier IC2B. The output of this amplifier is a voltage directly related to the instantaneous RF output frequency as programmed by the sweep ramp. This voltage ranges linearly from 0 V at 0 MHz to 2.5 V at 2500 MHz , and is not affected by the band or oscillator selection.

## BAND SWITCH PULSE

IC2A and its associated components form a pulse generator which puts out a $+18 \vee 1 \mathrm{msec}$ pulse whenever any of the $B-1, B-2 A, B-2 B$, or $B-3$ oscillator enable signals changes states. This pulse provides a 1 msec delay at the band switching crossover points (the delay circuit is in the M101B), and is used to generate the band stacking blanking and sequence sync pulses in the M132.

### 3.14 M132 - INTERFACE

This module accepts the band selection signals from either the front-panel BAND switch or the rear-panel PROGRAMMING jack and converts them, via switching transistors, into drive voltages for the M131 Band Select module. The M132 also takes the band switch pulse from the M131 and converts it into the positive and negative Z-axis pulses (for the rear-panel BAND STACKING BLANKING connector) and the sequence sync pulse available at pin 25 of the PROGRAMMING jack.


## SECTION PERFORMANCE TESTS

### 4.1 INTRODUCTION

The purpose of the performance tests in this section is to verify that the Model 2002A Sweep/Signal Generator meets its published specifications (Section 1.2). These tests assume that the instrument is equipped with Option A3, Deluxe Harmonic Markers (Sections 1.2.5 and 1.3.3). This option provides a selective combination of harmonic markers at $1,10,50$, and 100 MHz intervals throughout the 1 to 2500 MHz frequency range. While it is possible to check the instrument's performance without Option A3 by using suitable external CW sources, a complete check by this method is impractical. The Individual Harmonic Markers, Option A2, can be used up to 1500 MHz only, and are therefore inadequate.

Recommended test equipment is listed in Table 4-1. Tests are normally performed in the order listed. The order conforms to the Specification order in Section 1.2. If tests are performed on Option A3 (Section 4.13.4), the user may perform this test prior to other tests.

Refer to operating instructions in Section 2 to become familiar with Model 2002A controls and their functions prior to beginning these tests. Before applying AC power to the Model 2002A, see Section 2.3 for electrical installation details. The line voltage should be maintained at either 115 or 230 VAC $\pm 10 \%$, 50 to 400 Hz during the tests. The nominal ambient temperature for tests is $25^{\circ} \mathrm{C}$. Correction factors are to be applied as specified in some of the tests at different ambient temperatures.

## Table 4-1. Recommended Test Equipment

| INSTRUMENT | CRITICAL REQUIREMENT | RECOMMENDED |
| :---: | :---: | :---: |
| Oscilloscope | DC coupled, $1 \mathrm{mV} / \mathrm{div}$ sensitivity | HP-1200A |
| Digital Voltmeter | Accuracy: $\pm .04 \%$ | Dana 4200 |
| Power Meter | Frequency Range: 1 MHz to $\mathbf{2 5 0 0} \mathrm{MHz}$ | HP-435A/8482A |
| Spectrum Analyzer | Frequency Range: 1 MHz to 5 GHz | HP-8554B/8552B <br> HP-8555A/85552B |
| Precision Attenuator Pads | 10,20 and 40 dB | Weinchel 50-10, 50-20, 50-40 |
| CW Signal Generator | Adjustable from 1 MHz to 1600 MHz with 0.1 V output, Accuracy: $\pm 10 \mathrm{MHz}$ | Any suitable signal source covering this frequency range. |
| Marker Generator | 1,10,50,100 Harmonic Markers | Wavetek Option A3 |
| RF Detector | Frequency Range: 1 MHz to 2500 MHz | Wavetek D153 |
| Frequency Counter | Frequency Range: to 500 MHz | HP-5300B/5303B |
| VSWR Bridge | Frequency Range: 5 MHz to $2 \mathrm{GHz}, 40 \mathrm{~dB}$ directivity. | Wiltron 60N50 |

### 4.2 FREQUENCY RANGE AND ACCURACY TESTS

Mechanical dial check: rotate the Model 2002A CENT FREQ/START and SWEEP WIDTH/STOP thumb wheels to their mechanical stops at minimum frequency positions. Both frequency pointers must read $0 \pm 2 \mathrm{MHz}$ on the sweep width FREQUENCY SCALE. If they do not, see Section 5.3.3.

### 4.2.1 $\triangle F$ MODE

The frequency range and accuracy are measured using the setup in Figure 4-1. Set the Model 2002A controls as follows:

| BAND | 1 |
| :--- | ---: |
| CENT FREQ | 250 MHz |
| SWEEP WIDTH | 500 MHz |
| MODE | $\mathrm{\Delta F}$ |
| STEP ATTENUATOR | $+\mathbf{1 0 \mathrm { dBm }}$ |
| OUTPUT VERNIER | +3 dBm on METER |
| SWEEP TIME | $0.1-0.01 \mathrm{sec}$ |
| VAR/MANUAL | full cw |
| HARMONIC MARKERS | 50 MHz |
| MARKER WIDTH | WIDE |
| TILT/NORM | NORM |
| TRIG/RECUR | RECUR |
| SIZE | full down |
| BLANKING | ON |
| EXT/INT | INT |

The seven MARKER pushbuttons ape off (not depressed).
Set the scope's horizontal and vertical inputs for DC coupling. Turn on AC power, and allow the Model 2002A to stabilize for 30 minutes minimum.

Adjust the Model 2002A MARKER SIZE control and the scope's horizontal and vertical sensitivity controls to obtain a display similar to Figure 4-2.

## NOTE

Adjust the Model 2002A VAR/MANUAL control for optimum viewing on the scope. The sweep time should be fast enough to eliminate flicker, and slow enough to accurately identify the 0 MHz marker (lock-in point). Because of variations in detector, scope, and leveler responses, slight distortions may occur at the low-frequency end of the display. Viewing of the display may be enhanced by disconnecting the detector output from the DEMOD in connector. This provides a horizontal base line with markers. The zero lock-in point is enhanced by depressing the EXT MARKER pushbutton and turning the front-panel BLANKING switch off. The end points of the horizontal line are adjusted to coincide with the left and right graticule
borderlines using scope horizontal position and sensitivity controls. In this test and subsequent tests, use either the detected or the horizontal-line display as desired.

Locate the 500 MHz marker by counting from the zero lock-in point at the lower left corner of the display in 50 MHz steps. Increase the CENT FREO (left thumb wheel) control setting until the 500 MHz marker is centered in the display. The frequency (green) pointer should indicate approximately 500 MHz . Decrease the SWEEP WIDTH (right thumb wheel) control setting from 500 MHz toward 0 MHz , and adjust the CENT FREQ control until a display similar to Figure $4-3$ is obtained. Set the HARMONIC MARKERS switch to 1 MHz , and adjust the CENT FREQ and SWEEP WIDTH controls to position the 499 MHz marker on the left graticule borderline and the 501 MHz marker on the right graticule borderline. This provides a sweep width of 2 MHz .

## NOTE

Adjust the scope horizontal sensitivity and position controls for a display 10 divisions wide and align on the graticule.

If RF output level is normal (Section 4.9), and vertical deflection is less than 1 volt, check for a faulty detector or and uncalibrated scope.

Operator viewing may be enhanced by turning off blanking and by disconnecting the demodulated signal from the Model 2002A. A horizontal line with markers will then be displayed at the base line.

Set the HARMONIC MARKERS to 50 MHz , and adjust the CENT FREO control until the zero beat of the 500 MHz marker is centered in the display as shown in Figure 4-3. The green pointer on the FREQUENCY SCALE must indicate between 490 and 510 MHz at an ambient temperature of $25^{\circ} \mathrm{C}$.

## NOTE

If it is necessary to verify that a 500 MHz marker is centered in the display, inject the output of a CW signal generator into the MARKER IN connector of the Model 2002A, and depress the EXT MARKER pushbutton on the front panel. Tune the signal generator until the external marker coincides with the original marker in the display. The signal generator frequency should be 500 MHz . This procedure can be used to identify any marker in subsequent tests.

## NOTE

Allow $\pm 0.5 \mathrm{MHz}$ additional error for each degree ambient temperature difference from $25^{\circ} \mathrm{C}$ on bands 1 and 2 . For


Figure 4-1. Typical Test Set-up


Figure 4-2. Detected RF Display (Band 1)


Figure 4-3. Birdy Marker Display (2 MHz Sweep Width)
example, a $20^{\circ} \mathrm{C}$ ambient temperature increases the allowable error by 2.5 MHz at 500 MHz , and the required FREQUENCY SCALE reading should be between 487.5 and 512.5 MHz . On band 3, the temperature correction factor is $1.0 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$.

By adjusting only the CENT FREQ control to center markers on the display, continue to verify frequency accuracy at 50 MHz intervals between 450 and 50 MHz . The frequency (green) pointer must indicate the center frequency within $10 \mathrm{MHz}+0.5 \mathrm{MHz}{ }^{\circ} \mathrm{C}$ at each 50 MHz interval.

To verify the 1.0 MHz minimum frequency on band 1 , set the HARMONIC MARKERS switch to 1 MHz , and adjust the CENT FREQ control to position the first marker to the right of the zero lock-in point at display center. The centered marker is the 1 MHz marker, and it should be clearly visible in the display. (The flatness down to 1 MHz is measured in Section 4.11.)

Set the HARMONIC MARKERS switch to 50 MHz , and adjust the CENT FREQ control to position the zero lock-in point at display center. Disconnect the RF detector from the DEMOD IN connector to facilitate the adjustment. The green pointer must indicate $0 \pm 10 \mathrm{MHz}+0.5 \mathrm{MHz} /^{\circ} \mathrm{C}$ on the FREQUENCY SCALE.

Use a procedure similar to the one above to measure the frequency accuracy on bands 2 and 3 . The allowable error on band 2 is $\pm 20 \mathrm{MHz}+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$. Use the external marker as needed to identify marker center frequencies. On band 3, the accuracy is verified at 100 MHz intervals using the 100 MHz harmonic markers. The allowable error on band 3 is $\pm 20 \mathrm{MHz}+1 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$. Note that full sweep width spans only half the band.

Set the BAND switch to 4 and check the full 1 to 2500 MHz range at 100 MHz intervals. The allowable error is $\pm 50 \mathrm{MHz}$ plus the applicable temperature compensation factor ( 0.5 or $1.0 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$ ). Note that the maximum sweep width is approximately 500 MHz .

### 4.2.2 CW MODE

The procedure in Section 4.2.1 measures frequency accuracy at narrow sweep widths. Operation in CW is equivalent to zero sweep width in $\Delta F$, except that no markers appear and blanking is inactive. It is therefore unnecessary, unless desired, to measure frequency range and accuracy in CW mode.

### 4.2.3 S/S (START/STOP) MODE

The following test measure frequency range and accuracy in the S/S mode. Set the Model 2002A controls as follows:

BAND
START
0 MHz
STOP 500 MHz
MODE

Adjust other controls as in the $\Delta \mathrm{F}$ mode test (Section 4.2.1). Adjust the START and STOP controls until the 0 and 500 MHz markers coincide with the left and right graticule borderlines as shown in Figure 4-2. The red pointer, which indicates stop frequency, must read between 485 and 515 MHz on the FREQUENCY SCALE at $25^{\circ} \mathrm{C}$. Adjust the STOP control until the 450 MHz marker coincides with the right graticule borderline. The red pointer must read between 435 and 465 MHz on the FREQUENCY SCALE at $25^{\circ} \mathrm{C}$. Repeat the above test at each 50 MHz interval to the MHz lock-in point. The allowable error is $\pm 15 \mathrm{MHz}+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$ difference from $25^{\circ} \mathrm{C}$ ambient temperature.

Readjust the STOP control until the 500 MHz marker coincides with the right graticule borderline, and adjust the START control, if required, until the 0 MHz lock-in point coincides with the left graticule borderline. The start frequency (green) pointer must read between -15 and +15 MHz on the FREQUENCY SCALE at $25^{\circ} \mathrm{C}$. By adjusting only the START control to position the markers, repeat the above test at each 50 MHz interval to 500 MHz . The allowable error is $\pm 15 \mathrm{MHz}+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$.

Repeat the above tests on bands 2 and 3 at each 100 MHz interval. (Use 100 MHz harmonic markers.) The allowable error on band 2 is $\pm 30 \mathrm{MHz}+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$, and on band 3 , $\pm 30 \mathrm{MHz}+1 \mathrm{MHz}{ }^{\circ} \mathrm{C}$.

Set the BAND switch to 4 and check the full 1 to 2500 MHz range at 100 MHz intervals. The allowable error is $\pm 50 \mathrm{MHz}$ plus the applicable temperature compensation factor ( 0.5 or $1.0 \mathrm{MHz} /^{\circ} \mathrm{C}$ ).

### 4.3 SWEEP WIDTH TEST

Using the setup in Figure 4-1 and the control settings in Section 4.2.1, obtain a display as in Figure 4-2, with lower corners that coincide with the left and right graticule borderlines. Adjust the CENT FREO and SWEEP WIDTH controls until the 500 MHz marker coincides with the right graticule border line, and the 0 MHz lock-in point coincides with the left graticule borderline. The red pointer on the sweep width FREQUENCY SCALE must indicate $500 \pm 15$ $\mathrm{MHz}+0.5 \mathrm{MHz} /^{\circ} \mathrm{C}$ difference from $25^{\circ} \mathrm{C}$ ambient temperature.

Adjust the SWEEP WIDTH control to 100 MHz and the CENT FREQ control to 300 MHz . Adjust both controls until the 250 MHz marker coincides with the left borderline


Figure 4-4. Linearity Display (Band 1)


Figure 4-5. Linearity Display (Bands 2,3)
and the 350 MHz marker coincides with the right borderline of the graticule. The red pointer on the sweep width FREQUENCY SCALE must indicate $100 \pm 15 \mathrm{MHz}$ $+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$ difference from $25^{\circ} \mathrm{C}$ ambient temperature.

Set the HARMONIC MARKERS selector to 1 MHz . Adjust the CENT FREQ and SWEEP WIDTH controls for a sweep width of exactly 1 MHz at any center frequency between 1 and 500 MHz . Adjust the CENT FREQ control to center a 1 MHz marker on the display. Set the MARKER WIDTH control to produce a marker approximately 200 kHz wide on the display.

Next, adjust the SWEEP WIDTH control toward minimum. The 200 kHz wide marker should expand horizontally to fill the display. This procedure verifies minimum sweep width requirements.

Repeat the above procedures for bands 2, and 3. The allowable sweep width error is $\pm 30 \mathrm{MHz}+0.5 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$ difference from $25^{\circ} \mathrm{C}$ ambient on band 2 . On band 3 , the allowable error is $\pm 30 \mathrm{MHz}+1.0 \mathrm{MHz} /{ }^{\circ} \mathrm{C}$. Minimum sweep width should be 200 kHz on all bands. When checking 500 MHz sweep width on bands 2 and 3 , set the CENT FREQ control to any 50 MHz interval near the center of the band.

The frequency accuracy measured in the preceeding tests is closely related to display linearity, which is measured in the following test.

### 4.4 DISPLAY LINEARITY TEST

Display linearity is measured at the band limits in the $\mathrm{S} / \mathrm{S}$ MODE only. Use the setup in Figure 4-1, and set the controls as in Section 4.2.3, except adjust the scope horizontal position and sensitivity controls to over-sweep both ends of the graticule approximately $1 / 2$ division. Adjust the START and STOP controls until each marker in the comb (including the 0 and 500 MHz markers) coincides with its corresponding vertical graticule line within 0.1 division ( 0.5 minor division). This allowable error is equivalent to a $1 \%$ linearity. (See Figure 4-4.)

## NOTE

If the horizontal linearity of the scope is improperly calibrated, the above test is invalid. Refer to the scope linearity check in Section 5.3.3 in this manual.

Repeat the above procedure on bands 2 and 3. The allowable linearity error is $\pm 0.1$ division on all bands. (Use 100 MHz harmonic markers.) (See Figure 4-5.)

### 4.5 SPURIOUS SIGNAL TEST

### 4.5.1 HARMONICS AND NON-HARMONICS

A spectrum analyzer covering the range of 1 MHz to 5 GHz is required for this test. Measurements are made in accordance with instructions furnished with the analyzer. The Model 2002A is set to CW mode. All markers should be turned off. The RF output of the Model 2002A is connected to the RF input of the spectrum analyzer.

The second and third harmonics of the output signal are usually the main spurious signals on all bands. These harmonics should be at least 20 dB below the carrier between 1 and 10 MHz , and at least 30 dB below the carrier between 10 and 2500 MHz .

Non-harmonic spurious signals are generated by a heterodyne oscillator on band 1. These spurious signals should be at least 35 dB below the carrier in the band ( 1 to 500 MHz ), and at least 30 dB below the carrier outside the band. No non-harmonics should be detectable on bands 2 or 3 , since fundamental oscillators are used.

### 4.5.2 RESIDUAL FM TEST

A spectrum analyzer is used to measure residual FM. The residual FM should be measured at the maximum frequency in each of the bands, and at any other desired frequencies in the range of 1 to 2500 MHz . The Model 2002A is set to CW mode. All markers are turned off. The RF output of the Model 2002A is connected to the RF input of the spectrum analyzer, and is set to +13 dBm . The spectrum analyzer is tuned to the fundamental of the Model 2002A.

With the spectrum analyzer set according for 3 kHz bandwidth, internal scan mode, $10 \mathrm{kHz} /$ division scan width, $0.2 \mathrm{sec} / \mathrm{division}$ scan time, and $10 \mathrm{~dB} /$ division sensitivity, the residual FM should be less than 10 kHz peak-to-peak on bands 1 and 3 , and less than 20 kHz peak-to-peak on band 3. The peak-to-peak measurement refers to the difference between the maximum and minimum frequencies of the signal peak which is observed as horizontal jitter on the spectrum analyzer. (See Figure 4-6.)

### 4.6 FREQUENCY DRIFT TEST

Frequency drift should be measured at $500,100,1500$, and 2500 MHz (the highest frequency of each oscillator), and at any other desired frequencies between 1 and 2500 MHz . Use the setup and control settings of Section 4.2.1, except


Figure 4-6. Residual FM


Figure 4-7. Horizontal Output Waveform
calibrate the display's sweep width to exactly 1 MHz and center the marker (for example, 500 MHz ) on the display with the SWEEP TIME switch set to LINE. Read frequency drift directly from the scope display by noting the change in the marker's position with time. Each division represents 100 kHz . When reading drift over long periods of time, calibrate the display's sweep width to 5 MHz using 1 MHz harmonic markers. Next, turn off the 1 MHz markers and turn on the 10 MHz (or 50 MHz ) harmonic markers. Center a marker on the scope display and read drift as before, except 1 division now equals 500 kHz.

The maximum allowable drift on bands 1 and 2 is 100 kHz per 5 minutes, or 2 MHz per 8 hours. This specification applies after a one-hour minimum warmup at a constant ambient temperature, and allowing a 5 minute stabilizing period after a frequency change. On band 3, the maximum allowable drift is 200 kHz per 5 minutes, or 4 MHz per 8 hours.

### 4.7 BLANKING TEST

With the front-panel BLANKING switch turned on, the RF output in $S / S$ and $\Delta F$ modes is removed during the sweep retrace time to provide a zero-volt base line. Use the setup in Figure 4-1 and preset the controls as in Sections 4.2.1 or 4.2.2. The display should be as shown in Figure 4-2. Set the BLANKING switch to its up position, and verify that the zero-volt base line is removed from the display. Repeat this test on bands 2 and 3. Reset the BLANKING switch to ON.

### 4.8 OUTPUT IMPEDANCE AND SWR TEST

A 50 ohm SWR bridge, a spectrum analyzer, and a signal generator are required for this test.

The output impedance and SWR of the Model 2002A are measured in combination, and the result is expressed as return loss which may be directly converted to SWR. The Model 2002A and the signal generator, both operating in CW mode, are set to the same output level and test frequency. The system is calibrated with the test port of the SWR bridge open and a 0 dB return loss reference is set on the spectrum analyzer. The Model 2002A is then connected to the test port of the SWR bridge. The SWR of the Model 2002A is obtained from the return loss indication on the spectrum analyzer as the signal generator is tuned through the test frequency range. The return loss indication is disregarded at points where the two frequencies are exactly equal. The SWR should be less than 1.5:1 (return loss greater than 14 dB ) with the Model 2002A OUTPUT STEP ATTENUATOR set to 0 dBm (10 dB insertion loss). The SWR should be less than 1.3:1 (return loss greater than 7 dB ) with the OUTPUT STEP ATTENUATOR set to -10 dBm ( 20 dB insertion loss).

### 4.9 RF OUTPUT MAXIMUM LEVEL TEST

This measurement is made with a power meter. Set the power meter to its +15 dBm range. Set the Model 2002A controls as in Section 4.2.1, except set the MODE switch to CW. Connect the power sensor to the RF OUT connector of the Model 2002A. The power meter must read between +12.5 and +13.5 dBm . RF output flatness is measured in Section 4.11.

### 4.10 RF OUTPUT ATTENUATION AND ACCURACY TESTS

### 4.10.1 STEP ATTENUATOR

The Step Attenuator provides 70 dB of attenuation in 10 dB steps. The accuracy can be measured by using a suitable attenuation test set, or by directly substituting precision RF attenuator pads for each 10 dB step of the Attenuator. The difference between the two outputs represents the Attenuator error. An RF detector can be used to recover the signal at levels down to approximately -40 dBm . Below this level, an RF amplifier or a sensitive receiver (spectrum analyzer) must be used. The allowable error is $\pm 3 \%$ of the attenuation. The maximum error, which is at 70 dB , is $\pm 2.1 \mathrm{~dB}$. This error is produced by the Step Attenuator alone, and does not include the flatness or the OUTPUT VERNIER ATTENUATOR error.

### 4.10.2 VERNIER ATTEINUATOR

The accuracy of the OUTPUT VERNIER ATTENUATOR is measured using the power meter while operating the instrument in CW mode on band 1 at 250 MHz . With the OUTPUT STEP ATTENUATOR set to +10 dBm , adjust the VERNIER for a +3 dBm reading on the output METER. The power meter should read $+13 \pm 0.5 \mathrm{dBm}$. Using the OUTPUT VERNIER only, check the output METER readings in 1 dB steps between +3 and -10 dB . The power meter reading at each step should be within 0.5 dB of the indicated output level (the sum of the output METER reading and the OUTPUT STEP ATTENUATOR setting). The output is not specified below -10 dBm output METER readings.

### 4.11 RF OUTPUT FLATNESS TEST

Flatness is the variation in output amplitude versus frequency. It is normally measured with a power meter, but it can be measured with a broadband negative-polarity RF detector. The power meter method is preferred, since its flatness is better than most RF detectors. A power sensor is used with the power meter, and a calibration chart is affixed to the sensor. At the operating frequency, a calibration factor noted on the chart is set on the power meter's calibration factor control, and a corrected reading is obtained from the power meter.

The flatness is measured in the S/S mode with the SWEEP TIME switch set to MANUAL. The BAND switch is set to 4, and the VAR/MANUAL control is adjusted through its range. The SLOPE control must be adjusted for zero slope. The power meter is set to its +15 dBm scale and connected to the RF OUT connector of the Model 2002A.

To read flatness down to the 1 MHz minimum, first calibrate the scope display from 0 to 10 MHz as follows. Set the SWEEP TIME selector to LINE and set the START control to -10 MHz and the STOP control to +10 MHz . Turn off all markers and depress the EXT MARKER pushbutton to activate the 0 MHz marker. The 0 MHz marker should appear near the display center. Turn on the 10 MHz harmonic markers. Adjust the START control to position the 0 MHz marker on the left graticule borderline, and the STOP control to position the 10 MHz marker on the right graticule borderline. Turn off the EXT MARKER and turn on the 1 MHz harmonic markers. With the SWEEP TIME selector set to MANUAL, adjust the VAR/MANUAL control to position the zero beat of the 1 MHz marker approximately one division from the left borderline of the display graticule. Turn off the markers. Set the proper calibration factor and read the power meter. (The power meter will null if the VAR/MANUAL control is set to the zero beat of the 0 MHz marker.) Tune the 1 to 10 MHz range with the VAR/MANUAL control and note the power meter readings.

Set the START and STOP controls to 10 and 2500 MHz respectively. Tune the entire frequency range with the VAR/MANUAL control. Note the frequency where the maximum corrected power meter reading is obtained. Use the OUTPUT VERNIER to adjust the corrected output level to exactly +13 dBm at that frequency where the maximum output level occurs. Again tune the full range and note the minimum corrected power meter reading. A minimum reading of at least +12 dBm is required to meet the $\pm 0.5 \mathrm{~dB}$ flatness specification.

## NOTE

If a detected swept response is to be observed, the lowest detected output level should be at least $\mathbf{9 0 \%}$ of the highest detected level at sweep rates up to $100 \mathrm{MHz} / \mathrm{ms}$. At faster rates, the overall flatness may deteriorate slightly.

### 4.12 SWEEP TIME (HORIZONTAL OUTPUT) TEST

Connect the Model 2002A HORIZ OUT connector to the scope vertical input. Adjust the scope controls for an internally generated, automatic, line-triggered sweep of 2 $\mathrm{mV} /$ division, and a vertical sensitivity of $2 \mathrm{~V} /$ division. Set the Model 2002A BAND switch to 1 , the SWEEP TIME selector to LINE, and the TRIG/RECUR switch to RECUR (full down position). Adjust the scope's vertical position, horizontal position, and trigger level to obtain a waveform as shown in Figure 4.7.

Set the SWEEP TIME selector to $0.1-0.01 \mathrm{sec}$ and the VAR/MANUAL control fully clockwise. The wait time should disappear and the sweep time should be less than 10 ms with approximately equal sweep time (rising) and retrace time (falling) periods. Set the scope time base to $20 \mathrm{~ms} / \mathrm{division}$. Adjust the VAR/MANUAL control fully counterclockwise. The sweep time should be greater than 100 ms with approximately a 10:1 ratio between the sweep and retrace time periods.

## NOTE

The retrace time period remains fairly constant at any SWEEP TIME setting as the VAR/MANUAL control varies the total sweep time period. With the VAR/MANUAL control fully clockwise, the sweep and retrace times are both 0.01 seconds. With the control fully counterclockwise, the sweep time is approximately 0.1 seconds and the retrace time remains 0.01 seconds. On the next lower range ( 1 -. 1), the retrace time should be a constant 0.1 seconds, and the sweep time should vary from 0.1 to 1 second.

Repeat the previous checks for the 1-.1, 10-1, and 100 -10 second positions on the SWEEP TIME selector switch. Adjust the scope time base as necessary to ensure that the VAR/MANUAL control will adjust the sweep time from greater than the maximum to less than the minimum time specified for each range.

Set the SWEEP TIME selector to MANUAL and adjust the VAR/MANUAL control throughout its range. A DC voltage should be present at the HORIZ OUT connector that is variable from $0 \pm 0.5 \mathrm{~V}$ with the control fully counterclockwise to $+10 \pm 0.5 \mathrm{~V}$ with the control fully clockwise. Use a DVM for this measurement.

Set the SWEEP TIME selector to the $.1-.01$ position and the TRIG/RECUR switch to its middle position. The sweep should be disabled. Moving the TRIG/RECUR switch to the fuil up (spring-loaded) position and then releasing it should produce one complete sweep cycle.

## NOTE

The triggered mode of operation is possible only in the variable rate positions, and will not operate in the LINE or MANUAL positions of the SWEEP TIME selector.

### 4.13 MARKER SYSTEM TESTS

The Model 2002A utilizes a birdy-bypass marker system which provides for both internal and external markers. A CW signal generator is used to check out the external system. Option A3, which provides a combination of 1,10 , 50 , and 100 MHz harmonic markers, is required to fully check out the internal marker system.

A front-panel rotary switch (labeled HARMONIC MARKERS) selects the desired comb in Option A3. An internal operator control on module M105 (labeled Size Ratio) adjusts the ratio of small to full-size markers in the comb to facilitate identification in all marker options. Other markers, Options A1 and A2, if installed, and the external marker, are individually selected by label from the row of seven front-panel MARKER pushbutton switches. All marker geometries (size, width, tilt, and rectification) are controlled from front-panel switches and controls. In addition, all markers have internal Size controls (see Section 5.3.6 for adjustment procedure).

### 4.13.1 EXTERNAL MARKER

Use the setup in Figure 4-1 and connect the CW output of a signal generator to the Model 2002A MARKER IN connector. Set controls as in Section 4.2.3, and adjust the MARKER SIZE control to obtain a display similar to Figure 4-2. Set the signal generator for a 100 mV CW output, and depress the Model 2002A EXT MARKER pushbutton. Tune the signal generator from 1 to 500 MHz and note the movement of the external birdy in the display. The fundamental external birdy amplitude should be approximately equal to the amplitude of the even harmonic markers in the comb. The amplitude of second and thrid harmonics of the external signal, when in the band, may also be approximately equal to the fundamental marker amplitude.

When operating on band 2 or 3 , the second, third, or higher harmonics of the external signal generator carrier may be required to verify operation of the external marker system on signal generators with limited maximum frequency. Increasing the level of the carrier may be required.

### 4.13.2 SINGLE FREQUENCY MARKER (OPTION A1)

Use the procedure in the previous sections, and depress the correct pushbutton for the single frequency marker to be tested. Turn off all other markers, and set the BAND switch for the correct band to display the single frequency marker. Adjust the CENT FREO control to center the marker on the display, and read the FREQUENCY SCALE to identify the marker within 5 MHz .

### 4.13.3 INDIVIDUAL HARMONIC MARKERS (OPTION

 A2)Option A2 provides a harmonic marker comb up to 1500 MHz . Use the setup and procedure in Section 4.2.3, except depress the appropriate pushbutton in the row of MARKER switches ( 50 HAR, for example), and turn off all other markers.

The Option A2 markers can be tested using a procedure similar to Section 4.13.4, except the maximum operating frequency is 1500 MHz for the individual harmonic markers.

### 4.13.4 DELUXE HARMONIC MARKERS (OPTION A3)

The Option A3 harmonic markers are used in several previous performance tests. The $1,10,50$, and 100 MHz harmonic (comb) markers are controlled by the front-panel HARMONIC MARKERS rotary switch. To check out the Option A3 markers, proceed as follows.

## NOTE

The following tests for marker frequency accuracy, marker width, size, rectification and tilt are made with the 50 MHz harmonic markers. Other markers can be tested using a similar procedure.

## MARKER ACCURACY

Marker accuracy can be verified by any one of several methods. In one method, a frequency counter measures the RF output frequency of the Model 2002A as follows: A convenient harmonic marker (preferably near the counter's maximum frequency) or a single frequency marker is displayed on the scope with the Model 2002A operating in $\triangle F$ mode with a sweep width of approximately 1 MHz . The sween time is then set to MANUAL, and the VAR/MANUAL control is adjusted for a zero beat of the displayed marker. The marker's frequency is read on the frequency counter, For example, a 500 MHz marker should read $500 \mathrm{MHz} \pm 25 \mathrm{kHz}$. The allowable error is as follows: $0.005 \%$ at $25^{\circ} \mathrm{C}$ and $0.007 \%$ at 0 to $50^{\circ} \mathrm{C}$ for Options A1 and A2. For Option A3, the allowable error is $0.005 \%$ at 0 to $50^{\circ} \mathrm{C}$. Since the error is quite small, a higher harmonic frequency provides an error which is more easily read on the counter. On Option A3, a single crystal reference is used for all harmonic frequencies, and only a single measurement is required.

A second method uses a tunable frequency synthesizer as an external marker. With the Model 2002A operating in $\Delta F$ mode, a test marker is displayed at 1 MHz sweep width. The synthesizer is tuned until its zero beat coincides in the scope display with the zero beat of the test marker.

A third method uses a frequency counter only, but requires removal of the instrument and marker covers. A probe from the marker oscillator section to the counter is adjusted for a signal level sufficient for the counter to accurately read the crystal frequency.

The highest crystal frequency used in the Model 2002A is 50 MHz . Markers above 50 MHz use harmonics of a given crystal frequency.

Test equipment for marker accuracy is not listed in Table $4-1$, since the inherent stability of quartz crystals makes a marker accuracy check unnecessary in all but the most critical applications.

## MARKER WIDTH

Repeat the setup in Figure 4-1, and set the Model 2002A controls to position a 2500 MHz marker on the display at a sweep width of exactly 1 MHz . Other controls should be initially set as in Section 4.2.1. Adjust the MARKER SIZE control and scope vertical sensitivity for a 2 Vpp marker display.

Adjust the CENT FREQ control to center the marker's zero beat on the scope display. With the MARKER WIDTH switch set to WIDE, note that the displayed marker width is approximately 400 kHz (each horizontal division equals 100 kHz ). Decrease MARKER WIDTH in successive steps to NARROW, and note that the marker width decreases in steps to approximately 15 kHz at NARROW.

## NOTE

Marker width is also a function of internal marker Size controls. The above check applies to normal settings of internal marker controls.

## MARKER SIZE

Set Model 2002A controls as in Section 4.3.2, and observe the 50 MHz marker comb from 50 to 500 MHz . Note that even harmonic markers (100, 200, . . . etc.) have a uniform amplitude in the display. The odd harmonic markers (50, $150, \ldots$ etc.) have a smaller, but uniform amplitude. The relative amplitude or size is determined by the internal Size Ratio control (see Section 5.3.5). The even harmonic of the 50 MHz harmonic markers should be of uniform amplitude throughout all four bands. The odd harmonics should be smaller, but of uniform amplitude throughout all bands.

Set the MODE switch to $\triangle F$ and center the 2500 MHz marker on the display at a sweep width of approximately 2 MHz using the CENT FREQ and SWEEP WIDTH controls on band 3. Set the scope's vertical sensitivity and position controls as required to read marker amplitude in the following steps. With the front-panel SIZE paddle switch fully depressed (to the large diamond), rotate the MARKER SIZE control throughout its range. The displayed marker amplitude should vary from approximately 4 Vpp at the clockwise limit to
approximately 10 mVpp at the counterclockwise limit. Set the SIZE paddle switch to mid-position (small diamond). Again rotate the MARKER SIZE control throughout its range. The displayed marker amplitude should vary from approximately 25 mV pp to approximately $50 \mu \mathrm{Vpp}$.

## MARKER RECTIFICATION

Set the SIZE paddle switch to full up position (triangle). This position provides positive retified birdy markers for use with X-Y plotters. With the SWEEP TIME selector set to . 1 - .01, adjust the VAR/MANUAL control fully counterclockwise. Disconnect the RF detector from the DEMOD IN connector on the Model 2002A and rotate the MARKER SIZE control throughout its range. With the scope properly adjusted, the marker amplitude should vary from approximately 2 V to 1 mV . The rectified marker amplitude depends upon the RF detector impedance when connected to the DEMOD IN connector. With the DEMOD IN connector center conductor shorted to ground, the voltages should vary from approximately 0.2 V to 1 mV .

## MARKER TILT

Center the 2500 MHz marker in the display at a sweep width of approximately 200 MHz . Set the TILT/NORM switch to TILT and the SIZE paddle switch to full down position. While adjusting the MARKER SIZE control throughout its range, note that the marker is adjustable from a 4 Vpp nearly vertical marker to a horizontal marker equal to approximately $10 \%$ of the horizontal display (1 division of 10).

### 4.14 EXTERNAL PROGRAMMING

External programming inputs are not normally checked at incoming inspection unless these special functions are to used in a particular application. The program input signals, external controls necessary, and input pin connections are covered in Section 2, Operation. If it is necessary to check these functions at incoming inspection, reference can be made to that section of the manual for complete setup instructions.

### 4.15 SLOPE TEST

Set the BAND switch to 4 , the MODE switch to $S / S$, and the START and STOP controls to 1 and 2500 MHz , respectively. Use the OUTPUT VERNIER to calibrate levels of $7.5,+10$, and +12.5 dBm on the scope display (refer to Figure 4-7). Reset the OUTPUT VERNIER for a +10 dBm output ( 0 dBm on output METER). Use a screwdriver to adjust the front-panel SLOPE control fully clockwise. When viewed on the scope display, the output at 2500 MHz should be approximately +12.5 dBm and the output at 1 MHz should still be +10 dBm . Adjust the

SLOPE control fully counterclockwise. The output at 2500 MHz should be approximately +7.5 dBm and the output at 1 MHz should still be +10 dBm when viewed on the display. The sloped line should be approximately linear.

### 4.16 1 KHZ MODULATION TEST

Set the BAND switch to 4 , the MODE switch to $\mathrm{S} / \mathrm{S}$, the START control to 1 MHz , the STOP control to 2500 MHz , the SWEEP TIME selector to MANUAL, and the VAR/ MANUAL control fully ccw. Turn off all markers and blanking. Turn the 1 kHz MOD pushbutton switch on and set the scope for $0.2 \mathrm{msec} /$ division on the horizontal time base, internally triggered. A waveform (approximately square) with a period of 1 msec should be displayed. The
amplitude of the waveform should be equal to that of the unmodulated waveform. Tune the VAR/MANUAL control throughout its range and note the amplitude of the waveform at all frequencies. Turn the 1 kHz MOD switch off.

### 4.17 PEN LIFT (OPTION B4)

Two terminals are provided on the rear panel which provide contact closure during forward sweep time. Pen lift occurs only in the $1-10$ and $10-100$ positions of the SWEEP TIME control. The unit is tested with an X-Y plotter or with a VOM to indicate contact closure during the sweep trace interval. The marker SIZE paddle switch should be in its full up position when checking markers with an X-Y plotter:

### 5.1 INTRODUCTION

This section provides information for servicing, calibrating, and troubleshooting the Model 2002A Sweep/Signal Generator.

### 5.2 SERVICE INFORMATION

### 5.2.1 DISASSEMBLY INFORMATION

Refer to Figure 5-1.
REMOVAL OF BOTTOM COVER - Remove two rear feet (A) and lift cover off with a slight rear movement. Reinstall cover by reversing the removal procedure.

REMOVAL OF TOP COVER - Remove the single screw (B) from top and lift off cover with a slight rear movement. Reinstall cover by reversing the removal procedure.

REMOVAL OF SIDE PANEL - To remove the right side panel, refer to Section 5.2.3. To remove the left-side panel, remove the six screws ( $E$ ) holding the side panel to the instrument. However, one side panel must remain on the instrument to secure the front-panel assembly to the chassis.

## CAUTION

To prevent possible damage to harness when reinstalling side panels, use only the original screws or equivalent. Longer screws in the bottom two holes can cause damage to wiring.

### 5.2.2 MODULE SERVICING

REMOVAL OF MODULE - Modules may be replaced by removing any cables attached to top of the modules and
removing hold-down screw (C) from bottom. Rock module slightly while lifting upward to free module from chassis socket.

REMOVAL OF MODULE COVER - Remove all nuts and screws from top of module and slide cover off.

REINSTALLING MODULE - Before installing the module, check that module pins are straight and properly aligned; then carefully seat module pins into the chassis socket, replace module hold-down screw (C) to insure a good ground connection between module and chassis, and replace any cables attached to top of module. Module cable connections are shown in Figure 5-22.

## NOTE

If a defective module is replaced with a new module, certain calibration procedures must be repeated as shown in the following list:

| MODULE | PROCEDURE | SECTION |
| :--- | :--- | :--- |
|  |  |  |
| M101B | Sweep Rate | 5.3 .2 |
| M102A | Frequency Cal | 5.3 .3 |
| M103A | Frequency Cal | 5.3 .3 |
| M104A | Level Cal | 5.3 .4 |
| M105 | None | --- |
| M109 | Frequency Cal | 5.3 .3 |
| M110 | Frequency Cal | 5.3 .3 |
| MA111 | Level Cal | 5.3 .4 |
| M121 | 1 kHz Mod Adj | 5.3 .5 |
| M131 | Frequency Cal | 5.3 .3 |
| M132 | None | --- |
| M6C | None | --- |
| M6H | Marker Size | 5.3 .6 |
| M6S | Marker Size | 5.3 .6 |
| M106 | Marker Size | 5.3 .6 |



Figure 5-1. Disassembly


BOTTOM VIEW

Figure 5-2. Module Pin Configuration


Figure 5-3. Connector Alignment

SERVICE KIT K005 - This kit contains a module extender, RF extension cables, and adapters which enable a module to be electrically operated while physically located above the rest of the modules, thereby making all parts easily accessible.

MODULE-PIN NUMBERING SYSTEM - The module pins are numbered as shown in Figure 5-2. The off-center index stud prevents the module's being plugged in backward and also provides a method for locating pin 1.

## NOTE

All 16 pins are not required in each module. Only the pins actually used are installed, but the numbering system remains the same.

### 5.2.3 OUTPUT AMPLIFIER SERVICING (MA111)

Refer to Figure 5-22. First remove cable W2 from the Amplifier and the M110 Sweep Oscillator. Remove the sweep sample cable, W5, from the Amplifier, and remove the output cable W3 from the Step Attenuator. (Do not attempt to remove cable W3 from the Amplifier yet.) Next, remove the 6 screws holding the right-side panel to the instrument (screws ( $E$ ) in Figure 5-1). Do not remove the two screws in the side panel holding the Amplifier to the side panel. The right-side panel can now be removed from the instrument, which will provide access to the Amplifier. The Amplifier can be operated in this position by substituting for cable W2 with a longer flexible cable provided in the service kit. Remove cable W3 from the Amplifier output and connect an RF detector or power meter directly to the Amplfifier output to check its performance. To reinstall the Amplifier, reverse this procedure. Remember to securely tighten cable W3 to the Amplifier output before reinstalling the side panel.

### 5.2.4 POWER SUPPLY SERVICING

PRINTED CIRCUIT BOARD CONNECTORS - When reinstalling a harness connector to the Power Supply printedcircuit board, be sure connector is properly aligned with the board connector pins and that connector faces proper direction (see Figure 5-3).

POWER SUPPLY BOARD REMOVAL - The Power Supply board and heatsink can be removed by removing the four screws which secure the printed circuit board to the instrument rear panel. After removal of the connecting harnesses, the board can be carefully lifted from the instrument.

## CAUTION

The Power Supply board may be raised far enough to allow
checking of many components with the harnesses still connected; however, power must NOT be applied to the instrument unless the negative (ground) side of C10 is connected to the instrument chassis ground and to the positive (ground) side of C9 (jumper wires are sufficient).

The Power Supply board is reinstalled by reversing the removal procedure.

### 5.2.5 TRANSISTOR AND IC LEAD CONFIGURATION

Lead configuration is shown in Figure 5-4.

### 5.2.6 RECOMMENDED TEST EQUIPMENT

The test equipment shown in Table 4-1 is recommended for servicing, troubleshooting and calibrating the Wavetek Model 2002A.

### 5.3 CALIBRATION PROCEDURE

The following procedure assumes the instrument is equipped with the A3 Deluxe Harmonic Marker option. Calibration by using an external marker generator and other marker options is possible; however, a complete calibration by this method is extremely inefficient.

Figure 5-4. Component Lead Configuration

Remove top and bottom covers. The instrument is calibrated using the module extender from the service kit. Allow a half-hour warm-up before calibrating.

In general, calibration should be performed in the sequence given.

### 5.3.1 POWER SUPPLY CHECK AND ADJUSTMENT

The Power Supply provides +27 VDC (unregulated), and three regulated DC voltages, $+18 \mathrm{~V},-18 \mathrm{~V}$, and +7 V to the instrument. The performance of the Power Supply can conveniently be checked by measuring the values at J 2 . (See Figure 5-22 and Table 5-1.)

The Power Supply also supplies a 20 VAC signal on pin 8 of J 2 which is used to trigger the sweep rate circuit when the SWEEP TIME control is set to LINE.

A separate +20 V supply is used to the supply DC voltage to the MA111 Output Amplifier. It is located on the under side of the chassis as shown in Figure 5-23.

Adjust the +20 volt control to provide +20.0 volts at the indicated point in Figure 5-23. Typical peak-to-peak ripple is $<10 \mathrm{mV}$.

## MAINTENANCE



## TABLE 5-1. J2 PIN VALUES

| J2   <br> PIN SUPPLY TOLERANCE | TO-PEAK RIPPLE |  |  |
| :--- | :--- | :--- | :--- |
| 1 | +27 | $+28 \pm 1^{*}$ | 1.5 V |
| $2 \& 3$ | +18 | +18.00 ADJ | .5 mV |
| $4 \& 5$ | -18 | -18.00 ADJ | .5 mV |
| 6 | NC |  |  |
| 7 | +7 | $7.5 \pm .2$ | .5 mV |
| 8 | 20 VAC | ------- | -------- |

*With input 115 VAC

### 5.3.2 SWEEP RATE ADJUSTMENT AND CHECKS

The sweep rate circuit consists of module M101B and associated front-panel controls. It provides the basic ramp from which the horizontal output and sweep drive signals are derived, plus the RF blanking signal and a precision $\pm 10 \mathrm{~V}$ supply. The following procedure checks and calibrates the sweep rate circuit.

## DISASSEMBLY PROCEDURE

Remove the screw from the top of module M101B and lift cover off. Figure $5-5$ shows the location of the M101B adjustments. Figure $5-6$ shown the associated front-panel controls.

## FREQ ADJUSTMENTS

Set the instrument control as follows:

| MODE | $\Delta F$ |
| :--- | :--- |
| BAIND | 1 |
| SWEEPTIME | $.01-.1$ |
| VAR/MANUAL | full cW |
| TRIG/RECUR | RECUR |
| BLANKING | ON |
| SWEEP DWELL | OFF |

Connect the oscilloscope's vertical input to the HORIZ OUT connector on the instrument front panel. Adjust the oscilloscope's sensitivity, position, and time base controls to produce a stable pattern similar to Figure 5-7. Adjust the Freq adjustment in the M101B module to produce a sweep time of $\leqslant 10 \mathrm{msec}$. Set the MANUAL control fully counterclockwise and check the sweep time. It must be longer than 110 msec .

## WAIT TIME ADJUSTMENT

Set the instrument controls as follows:

| MODE | $\triangle F$ |
| :--- | :--- |
| BAND | 2 |
| SWEEP TIME | LINE |
| VAR/MANUAL | N/A |
| TRIG/RECUR | RECUR |
| BLANKING | ON |
| SWEEP DWELL | OFF |
| CENT FREQ | 1000 MHz |
| SWEEP WIDTH | 500 MHz |

The scope should show a triangle wave with a delay of approximately 1 msec in approximately the center of both the rise and fall of the waveform (see Figure 5-7). These delays are due to band switching discontinuities. Adjust the Wait control (located on the rear of the SWEEP TIME switch - see Figure 5-22) to produce a 1 msec delay at the bottom of the triangle (see Figure 5-8).

Set the BAND switch to 1 . The wait time at the bottom of the triangle should be approximately 3 msec with no delays due to band switching discontinuites. The same should be true when the BAND switch is set to 3 .

Set the BAND switch to 4. The rise and fall times of the triangle should be approximately twice as long as they were on Band 2, thus the repetition rate is half the line frequency. The wait time should vary from approximately 1 to 7 msec , depending upon the number of band switching discountinuity delays present as the CENT FREO and SWEEP WIDTH control settings are varied.

## MANUAL LIMIT ADJUSTMENT

Set the front-panel SWEEP $\boldsymbol{T}^{-1 M E}$ selector to its MANUAL POSITION. Set the scope's horizontal trigger control for line rate. Set the VAR/MANUAL control fully clockwise and adjust the Manual Limit control on the M101B to produce a DC voltage exactly equal to the peak amplitude of the horizontal output as read in Figure $5-7$ or $5-8$ (approximately +10 V ).

## SWEEP DWELL

Set the BAND switch to 4 and turn the rear-panel SWEEP DWELL switch on. The wait time at the bottom of the triangle should increase by approximately 4 msec . The fall time of the triangle wave should decrease, thus the repetition rate of the sweep remains at half the line frequency.

Set the BAND switch to 1,2 , or 3 . The rise and fall times of the triangle wave should be the same as they were


Figure 5-5. M101B Adjustments


Figure 5-7. Frequency Adjustment


Figure 5-9. Ramp Size Adjustment


Figure 5-6. Sweep Time Controls (F.P.)


Figure 5-8. Wait Time Adjustment


Figure 5-10. Tape Drive
previously, but the wait time will increase by approximately 4 msec , thus cutting the repetition rate in half due to the wait time overlapping the line trigger pulse.

## PRECISION $\pm 10$ V SUPPLY CHECK

In order to maintain the accuracy of the FREOUENCY SCALE in the S/S, $\triangle F$ and CW modes of operation, the $\pm 10 \mathrm{~V}$ supplies, the standard-sweep ramp, and the inverted sweep ramp must maintain precise relationships with each other. These relationships are maintained by precision resistors and a single potentiometer (V Ramp Size) located in the M101B module. The following procedure checks these relationships and provides a high-resolution method of calibrating the inverted ramp size.

Connect the DVM to pin 7 of the M131 module. Set the BAND switch to 1 , the MODE switch to CW, and the CENTER FREO control against its mechinical stop at the low end of the FREQUENCY SCALE. Record the voltage read on the DVM to three decimal places. Set the CENTER FREO control against its mechanical stop at the high end of the FREQUENCY SCALE. Compare this voltage (ignoring polarity) to the previously read voltage. The difference should be less than 10 mV .

## RAMP SIZE CHECK

Set the instrument controls as follows:

| BAIND | 1 |
| :--- | :--- |
| SWEEP TIME | LINE |
| MODE | $\Delta F$ |

CENTER FREO and SWEEP WIDTH controls set against their mechanical stops at the high end of the FREOUENCY SCALE.

Connect the instrument HORIZ OUT connector to the oscilloscope's horizontal input. Adjust the oscilloscope to operate in an $X-Y$ mode with its horizontal sensititity set to 1 volt per division and the vertial sensitivity set to 50 millivolts per division. Center the trace on the scope with the position controls as shown in the dashed line of Figure 5-9. Connect the oscilloscope's vertical input to pin 7 of the M131 module. Set the SWEEP TIME selector to the 1 10 sec position and the VAR MANUAL control fully clockwise. (This slow sweep is necessary to prevent scope errors due to overdriving.) A trace with a repetition rate of 1 second should appear at the left side of the scope display (see Figure 5-9). The end of the scope trace should be 0 volts $\pm 70 \mathrm{mV}$ measured on the vertical axis. Do not change the setting of the SWEEP WIDTH control, but set the CENT FREQ control against its mechanical stop at the low frequency end of the FREOUENCY SCALE. The end of the scope trace should now be at the right side of the display (Figure 5-9) and again have an amplitude of 0 V +70 mV.

INVERTED RAMP SIZE (V RAMP SIZE)
Remove the vertical input to the oscilloscope. Set the SWEEP TIME to MANUAL. Adjust the VAR/MANUAL sweep time control to position the dot to the exact center of the oscilloscope display. Set the MODE switch to CW and both CENT FREQ and SWEEP WIDTH controls against their mechanical stops at the high end of the FREQUENCY SCALE.

Connect the DVM to pin 7 of the M131 module and record the voltage to three decimal places. Set the MODE switch to S/S and compare the DVM reading to the previously recorded voltage. The difference should be less than 35 mV . Record the second voltage to three decimal places. Rotate the VAR/ MANUAL control to its extreme counterclockwise position. Adjust the $V$ Ramp Size control in module M101B (see Figure 5-5) to obtain the same exact voltage. Rotating the VAR/MANUAL control through its entire range should not change the DVM reading. Replace the cover on the M101B module.

This procedure ensures the frequency error produced by module M101B will be less than 3 MHz .

### 5.3.3 FREQUENCY ADJUSTMENT

MECHANICAL ADJUSTMENT OF FREQUENCY INDICATOR TAPE

Rotate both START and STOP thumbwheels to their lowest frequency positions at the mechanical stops. Both frequency indicators must read $0 \mathrm{MHz} \pm 2 \mathrm{MHz}$ when read on the Sweep Width FREOUENCY SCALE: if not, proceed as follows: With reference to Figure 5-10, disengage Idler by forcing Idler Spring to a disengaged position. While Idler is disengaged, rotate the Tape Drive Gear until the frequency indicator indicates zero frequency. Release the Idler Spring and engage the Idler. If the frequency error is still more than 2 MHz , loosen the screw holding the Tape Guide and Rotate the Guide so the Tape can be disengaged from the sprockets on the Tape Drive Gear. Disengage the Tape from the Tape Drive Gear sprockets and advance the tape one sprocket in the opposite direction of the frequency error. Engage the Tape on the sprocket, reposition the Tape Guide and tighten the screw. Again disengage the Idler and turn the Tape Drive Gear to indicate zero frequency. The front-panel CENT FREQ/START control thumbwheel must be held against its mechanical stop during the entire adjustment procedure.

## OSCILLOSCOPE LINEARITY CHECK

Before making the following electrical adjustment, first check the horizontal linearity of the oscilloscope, since any oscilloscope linearity errors will be added to the linearity adjustment error.


Figure 5-11. Scope Linearity Check


Figure 5-12. Sweep Drive Adjustments

Adjust the oscilloscope to operate in an $\mathrm{X}-\mathrm{Y}$ mode and set the horizontal and vertical sensitivities to $1 \mathrm{~V} /$ division. Connect the instrument HORIZ OUT connector to the oscilloscope's horizontal input, and the VERT OUT connector to the oscilloscope's vertical input. The scope inputs should be DC coupled.

Set the instrument controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | $\triangle F$ |
| CENT FREQ | 250 MHz |
| SWEEP WIDTH | 100 MHz |
| SWEEP TIME | LINE |
| HARMONIC MARKERS | 50 MHz |

Adjust the oscilloscope's horizontal position and sensitivity controls for a horizontal line that over-travels the scope graticule approximately 0.5 division on both ends (see Figure 5-11). Adjust the MARKER WIDTH for a display width that slightly overlaps the width of a graticule line. Fine adjust the CENT FREO and SWEEP WIDTH controls until the 200 MHz marker exactly coincides with the extreme left graticule line and the 250 MHz marker exactly coincides with the center line of the scope graticule as shown in Figure 5-11. Disregard the position of the 300 MHz marker. Adjust only the CENT FREQ control until the 200 MHz marker coincides with the graticule line one division from the extreme left. The 250 MHz marker should coincide with the first graticule line to the right of center within $\pm .25$ minor division. Continue to adjust only the CENT FREQ control to position markers at one division intervals until the 200 MHz marker coincides with the graticule center line.

The 250 MHz marker should coincide with its corresponding graticule line within $\pm 0.25$ minor divisions at all five check points across the display.

The 0.25 minor division error ( 50 mV ) is equivalent to a $0.5 \%$ linearity error. This error can be eliminated by using the same scope for calibration and operation.

## ELECTRICAL FREQUENCY ADJUSTMENTS

Electrical frequency adjustments are located in modules M131, M102A and M103A. In order to access the controls in these modules, the module being adjusted should be set up on a module entender (part of Service Kit K004) with the module cover removed.

## LINEARITY REFERENCE ADJUSTMENT

Set the instrument controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | $\triangle F$ |
| CENT FREQ | exactly 250 MHz |

SWEEP WIDTH
SWEEP TIME
exactly 500 MHz LINE

Adjust the oscilloscope to operate in an $\mathrm{X}-\mathrm{Y}$ mode and set the horizontal and vertical sensitivities to $1 \mathrm{~V} /$ division. Connect the instrument HORIZ OUT connector to the oscilloscope's horizontal input and position the trace as shown in Figure 5-13. The scope trace must be exactly 10 divisions long, starting exactly on the extreme left graticule line and ending exactly on the extreme right graticule line. Adjust the oscilloscope's horizontal sensitivity and position controls as necessary. Connect the oscilloscope's vertica! input to Test Point A (see Figure 5-12) of module M102A.

Adjust the + Lin Ref Control to position the "knee" exactly one division from the extreme right side of the display (see Figure 5-13). Next, connect the oscilloscope's vertical input to Test Point B and adjust the - Lin Ref control to position the "knee" exactly one division from the extreme left side of the display (see Figure 5-13).

## CENTER FREQUENCY ADJUSTMENT

Set the instrument controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | $\triangle F$ |
| CENT FREQ | exactly 250 MHz |
| SWEEP WIDTH | 10 MHz |
| SWEEP TIME | LINE |
| HARMONIC MARKERS | 50 MHz |

Adjust the oscilloscope to operate in an $\mathrm{X}-\mathrm{Y}$ mode and set the horizontal and vertical sensitivities to $1 \mathrm{~V} /$ division. Connect the instrument HORIZ OUT connector to the oscilloscope's horizontal input and center the horizontal trace on the scope.

Connect the instrument's VERT OUT connector to the oscilloscope's vertical input and adjust the MARKER SIZE and WIDTH controls for a display similar to that shown in Figure 5-14. If no marker is visible on the display, increase the SWEEP WIDTH control until a small marker is present on the display. (The operation is such that odd harmonics of 50 MHz will have a smaller amplitude than even harmonics. Since the center frequencies of bands $1,2 \mathrm{~A}$, and 2 B are odd harmonics, they will have a smaller amplitude, while the center frequency of band 3 is an even harmonic and will have a larger marker amplitude.) This procedure will work if the center frequency error is less than 100 MHz . If the center frequency error is more than 100 MHz , an external marker must be used to identify the correct 50 MHz harmonic. The external marker generator's frequency can be at the center frequency or at a subharmonic. For example, the band 3 center frequency is 2000 MHz , so the external marker frequency can be 2000 , 1000 , or 500 MHz . The external marker circuit will produce harmonics of the input signal to 2000 MHz .

Figure 5-13.
Linearity Reference Adjustment

Figure 5-14.
Centering

Figure 5-15.
Display Calibration


## CENTERING BAND 1

With the M103A Centering Band 1 control (see Figure $5-12$ ) adjust the 250 MHz marker to the center of the display as shown in Figure 5-14. Decrease the sweep width to $<10 \mathrm{MHz}$ before completing the adjustment.

CENTERING BAND 2
This will be covered in the Linearity Adjustment (Band 2) Section below.

## CENTERING BAND 3

Set the BAND switch to 3 and center the 2000 MHz marker on the display with the Centering Band 3 control. Without touching other controls, switch between bands 1 and 3 and verify that each marker is centered.

## ADJUSTMENT OF O MHZ LOCK-IN POINT

Set the instrument controls as follows:

| BAND | 1 |
| :--- | :---: |
| MODE | $\Delta F$ |
| CENT FREQ | 0 MHz |
| SWEEP WIDTH | 10 MHz |

Adjust the M102A Sweep Width Band 1 control (see Figure $5-12$ ) to position the 0 MHz lock-in point to the exact center of the display.

Set the instrument controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | $\triangle F$ |
| CENT FREQ | exactly 250 MHz |
| SWEEP WIDTH | 530 MHz |
| SWEEP TIME | LINE |
| HARMONIC MARKER | 50 MHz |

With the oscilloscope's horizontal position and sensitivity controls, superimpose the 0 MHz lock-in point exactly on the extreme left graticule line and the 250 MHz marker exactly on the center line of the scope graticule. (Disregard location of all other markers.) See Figure 5-15.

## LINEARITY ADJUSTMENT (BANDS 1 AND 3)

Being careful not to disturb the oscilloscope's position and sensitivity controls, readjust the M102A Sweep Width Band 1 control to superimpose the 150 MHz marker exactly on the scope graticule line as shown in Figure 5-16. Proceed to adjust Band 1 Lin 1 through 9 controls in Module M102A
(Figure 5-12) to position each marker as shown in Figure 5-16. (There is no Lin 6 control for Band 1.) The adjustment procedure must be done in the sequence given.

Each of the eleven markers in the display must be aligned within $\pm .1$ full division of its vertical graticule line to provide the maximum specified linearity error of $1 \%$.

Set the MODE switch to S/S and adjust the START and STOP controls to exactly duplicate the display shown in Figure 5-16.

## Change to band 3 .

Turn on the 100 MHz markers. Check the position of the 2000 MHz marker. Adjust the Sweep Width Band 3 and Linearity controls (Lin 1 through 9) to position the markers as shown in Figure 5-16. (Use the Sweep Width Band 3 control to set the 1900 MHz marker.)

While observing the oscilloscope display, switch between bands 1 and 3 without adjusting any other controls. There should be a negligible shift in marker location on the display.

Set the oscilloscope's vertical sensitivity control for $5 \mathrm{~V} /$ division and connect the oscilloscope's vertical input to pin 7 of the M131 module.

## LINEARITY ADJUSTMENT (BAND 2)

Set the BAND switch to 2. With the oscilloscope's vertical input still connected to pin 7 of the M131 module, adjust R36 in the M131 to position the band 2A portion of the ramp such that it crosses 0 V exactly 2.5 divisions in from the extreme left graticule (see Figure 5-17). Adjust R42 such that the band 2 B portion crosses 0 V exactly 2.5 divisions in from the extreme right graticule. Turn on the 50 MHz markers and connect the oscilloscope's vertical input to the instrument's SCOPE VERT connector. Using the M103A Cent 2A control, position the 750 MHz marker exactly 2.5 divisions in from the extreme left graticule. Using the Sweep Width 2A control, position the 700 MHz marker exactly 2 divisions in from the extreme left graticule. Adjust the Band 2A Lin Adj controls to position the other markers at 0.5 division intervals (see Table 5-2).

Using the M103A Cent 2B control, position the 1250 MHz marker exactly 2.5 divisions in from the extreme right graticule. Using the Sweep Width 2 B control, position the 1200 MHz marker exactly 3 divisions in from the extreme right graticule. Adjust the Band 2B Lin Adj controls to position the other markers at 0.5 division intervals (see Table 5-2 and Figure 5-17).

Figure 5-16. Linearity Adjustments, Bands 1 And 3

Figure 5-17. Linearity Adjustments, Band 2

Figure 5-18. Linearity Adjustments, Band 4


TABLE 5.2. BAND 2 LINEARITY ADJUSTMENT
(Adjust controls in order given.)

BAND A

| CTL | MKR (MHz) | CTL | MKR (MHz) |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| 1 | 800 | 1 | 1300 |
| 2 | 850 | 2 | 1350 |
| 3 | 900 | 3 | 1400 |
| 4 | 950 | 4 | 1450 |
| 5 | 000 | 5 | 1500 |
| 6 | 650 | 6 | 1100 |
| 7 | 600 | 7 | 1050 |
| 8 | 550 | 8 | 1000 |
| 9 | 500 |  |  |

Replace the covers on modules M102A and M103A.
BAND 4 SET-UP

Set up of band 4 is a special case since this is a stacked band made up of four individual oscillators which have already been set up for linearity.

All controls for setting up band 4 are located in module M131 (see Figure 5-19). These controls act to break the basic ramp from the M101B rate generator into 4 sequential 10 V ramps before it is applied to the shaping circuits.

Place the front-panel BAND switch to 4, leaving the other front-panel controls and scope settings as they were for the Band 3 linearity adjustments. Using R57 in the M131, set the first crossover point approximately 2 divisions in from the extreme left graticule. Use R60 to set the second crossover 4 divisions in from the extreme left graticule and R64 to set the last crossover 6 divisions in from the extreme left graticule. These settings are approximate, and the crossover points may be moved slightly during the rest of this set-up to examine any oscillator at the point of crossover. Final setting of these crossover points will be covered in the next section. The reason for making these preliminary settings is to ensure that all four oscillators are activated in their appropriate sequence (see Figure 5-18).

Using R34, adjust the 250 MHz marker to fall precisely one division in from the extreme left graticule. (This must be the first centering control adjusted, as it affects the centering of all four oscillators.) Using R45, adjust the 750 MHz marker to be precisely on the 3rd graticule in from the oscilloscope's far left graticule. (To identify markers on bands other than band one, use the MARKER IN connector in conjunction with an external source.) Adjust R44 such that the 1250 MHz marker falls exactly on the center graticule of the scope. Adjust R40 such that the 2000 MHz marker falls on the second graticule in from the extreme right scope graticule. The four oscillators should
now be centered in their respective positions.
All that remains is to set the sweep widths of the oscillators such that the 500 MHz harmonics $(500,1000,1500)$ fall at the crossover points.

In setting the sweep widths, R17 must be adjusted first, as it affects all four oscillators. R17 adjusts the sweep width of the band 3 oscillator ( $1500-2500 \mathrm{MHz}$ ). To adjust, first move the last crossover point (with R64) slightly to the left of it's normal position (1 division to right of scope center), then adjust R17 to position the 1500 MHz marker from the band 3 oscillator on (or very slightly to the right of) the first graticule to the right of scope center.

R18 adjusts the sweep widths of the oscillators for bands 1, 2 A , and 2 B simultaneously. Adjust R18 to almost superimpose the 500 MHz marker from band 1 on the 500 MHz marker from band two (these markers can be seen simultaneously if the BLANKING switch on the front panel is turned off, since the crossover point on the retrace occurs at a lower frequency than it does during forward sweep).

If all of the aforementioned adjustments are properly made, there should be less than 20 MHz overlap of frequencies at any crossover point. The next section details the procedure for checking the overlap and making the final settings of the crossover points.

## CROSSOVER ADJUSTMENT

Set the BAND switch to 4. Adjust R57 in module M131 such that the first crossover point ( 500 MHz ) on the forward sweep (not the retrace) is exactly 2 divisions in from the left edge of the display. Adjust R60 such that the second crossover point ( 1000 MHz ) is exactly 4 divisions in from the left edge of the display. Adjust R64 such that the third crossover point ( 1500 MHz ) is exactly 6 divisions in from the left edge of the display.

After adjusting the crossover points, set the START and STOP controls such that the 450 MHz marker falls on the far left vertical graticule and the 550 MHz marker falls on the far right vertical graticule. Turn on the 10 MHz markers, and identify each marker by counting from the 450 MHz and 550 MHz markers toward the center of the display. (Do not count past the crossover point from either direction.) Adjust R57 in module M131 such that the crossover point is just to the left of the 500 MHz marker from the higher band (see Figure 5-18). The marker to the left of the crossover point should be 490,500 , or 510 MHz from the lower band. If it is not, adjust.

## NOTE

The exact frequency of the crossover point is not critical; however, the crossover "overlap" specification of $+20-9$ MHz should be maintained.


Figure 5-19. M131 Adjustments


Figure 5-20. M104A Adjustments


Figure 5-21. M121 Adjustments

Repeat the above procedure using the corresponding frequencies and controls for the 1000 and 1500 MHz crossover points.

Carefully replace the cover on the M131 module.

### 5.3.4 LEVEL ADJUSTMENT

The leveler adjustments and the output METER calibrator are located in modules M104A and M121. Remove the covers from these modules.

## SLOPE ADJUSTMENTS

The Model 2002A has two slope adjustments. The internal Slope control is factory set to compensate for any roll-off of amplitude due to components. The front-panel SLOPE control is for customer use to compensate for any roll-off due to interconnections. This slope is detectable on the output meter at slow sweep speeds, but since the purpose of the internal Slope is to assure a flat output, this slope is nulled out at the METER by the following procedure.

Set the Model 2002A for a sweep time of .01 seconds, sweeping from 1 to 2500 MHz (band 4, S/S). Connect the oscilloscope vertical input to pin 12 of the M121 module and adjust the internal Slope control (R9 of the M121) for zero slope. Connect the oscilloscope vertical input to pin 10 of the M121. Any slope showing at this point is now due entirely to the external scope control. Adjust the front-panel SLOPE control to obtain zero slope at this point. Now readjust the internal Slope control in the M121 to obtain the maximum slope. This slope is now due entirely to the internal slope. Set the front-panel SWEEP RATE control to MANUAL and rotate the VAR/MANUAL control throughout its range. The METER may show some deflection as the unit is swept manually. If it does, turn the VAR/MANUAL control fully cw and adjust the Meter Null control (R11 in the M104A) to bring the MIETER reading back towards its position when the VAR/MANUAL control is fully ccw .

It may be necessary to manually sweep the unit back and forth through its range several times while this adjustment is being made. Continue adjusting until the METER shows no perceptable deflection as the unit is manually swept through its range. The internal slope is now nulled out and will not show perceptably on the METER.

Switch the front-panel SWEEP RATE switch back to the .01 sec position and readjust the internal Slope control to obtain a flat output.

## METER CAL

With AC power turned off, check position of the METER pointer. It should be positioned over the dot at the
extreme left and of the METER scale. If not, the METER's mechanical zero must be readjusted.

Remove the two screws from the METER mounting bracket located on the back of the front panel. Remove the METER from the front panel. The METER's zero adjustment is now accessible, and can be adjusted for proper zero position. Reinstall the METER.

Turn AC power on and adjust the front-panel OUTPUT VERNIER control to the maximum clockwise position. Adjust the M104A Meter Cal control (see Figure 5-20) to superimpose the METER pointer over the +3 dBm mark at the extreme right side of the scale.

## SWEEP SAMPLE LEVEL ADJUST

Referring to Figure 5-22, disconnect cable W5 from the MA111 Output Amplifier. Connect the power meter's sensor to this sweep sample connector. Necessary coax adapters to connect the power sensor (type N) to the sweep sample connector (type SMC) are available as part of the K005 Service Kit. Adjust the Model 2002A controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | S/S |
| START | 0 MHz |
| STOP | 500 MHz |
| SWEEP TIME | MANUAL |

Rotate the VAR/MANUAL control to its center position and adjust the sweep sample SS Level control (R2) in module M104A (Figure 5-20) to obtain a power meter reading of -10 dBm . Rotate the VAR/MANUAL control through its entire range. The minimum and maximum readings must be between -8 and -12 dBm . Repeat this check for bands 2 and 3. Disconnect the adapters and reconnect cable W5 to Output Amplifier MA111.

## OUTPUT LEVEL MIN AND MAX ADJUST

Adjust the Model 2002A controls as follows:

| BAND | 1 |
| :--- | :--- |
| MODE | CW |
| CENT FREQ | 250 MHz |
| OUTPUT STEP | +10 dBm |
| OUTPUT VERNIER | full cw |

Set the power meter to its +15 dBm range and connect it to the instrument RF OUT connector. Adjust the Level Max control (R12) in module M104A to produce a power meter reading of +13 dBm .

Turn the OUTPUT VERNIER control to indicate -10 dB on the output METER scale. Set the power meter to its 0
dBm scale and adjust the Level Min control (R23) in module M104A to produce a power meter reading of 0 dBm . Since some interaction exists between the Level Max and Min controls, the adjustments must be repeated until the +13 and 0 dBm readings are obtained without further adjustments of the Max and Min controls. The RF output at other frequencies will be checked during Performance Tests (Section 4).

Replace the cover on module M104A.

### 5.3.5 1 KHZ MODULATION FREQ ADJUSTMENT

A single-turn potentiometer on top of module M121 (see Figure 5-22) adjusts the modulation frequency.

### 5.3.6 MARKER SIZE ADJUSTMENT (OPTION A1, A2, AND A3)

Each marker module has a Size adjustment potentiometer which is accessible from the under side of the sweep generator when the bottom cover is removed (see Figure 523). The control is adjusted until a saturated marker is obtained on the scope display. A saturated marker is obtained when a further increase in the marker module's Size adjustment does not increase the marker amplitude on the scope display. Increasing the Size adjustment beyond this point will result in spurious markers on the display.

The A3 Deluxe Harmonic Marker option has 4 Marker Size adjustments, one for each marker. They are normally adjusted while operating on band 4 . Check all bands and the entire frequency range for proper operation. The A2 Harmonic Marker options are adjusted while operating on band 3, and checked for proper operation on bands 1, 2, and 3 only.

An additional marker size control labeled "Size Ratio", located on top of module M105, is considerad an operator control. The Size Ratio control adjusts the ratio of small to full-size markers from approximately 25 to $80 \%$. It is normally adjusted for a $50 \%$ ratio (see Section 1.2 .5 ). This control also affects the full-size marker amplitude slightly.

### 5.4 TROUBLESHOOTING

Effective troubleshooting requires a thorough understanding of the block diagrams and circuit description located in Section 3 of this manual. The Performance Tests in Section 4 and Calibration Procedures in Section 5 will aid in localizing the trouble symptom to a particular module or PC board. Once this has been accomplished, the module or board can be replaced or repaired with aid of the proper schematic and parts layout diagram. In general, it is preferable to replace a defective module or PC board assembly.

Equipment troubles are frequently due simply to improper control settings; therefore, before engaging in a troubleshooting procedure, be sure the front-panel controls are set in proper operating position. Refer to the operating instructions in Section 2 of this manual for a complete explanation of each control's function along with typical operating instructions.

After verifying that the trouble is not improper setting of the controls or test setup, make a thorough visual inspection of the instrument for such obvious defects as loose or missing screws, broken wires, defective module-pin sockets, loose RF cables, and burned or broken conponents.

After localizing the problem, voltage and resistance checks will help find defective components.

For troubleshooting purposes, it is permissible to operate the Model 2002A with any of the plug-in modules or RF cables removed; however, the instrument should be turned off when removing or installing modules. If substitute modules are available, possibly from another Model 2002A, this provides an easy method of verifying if a suspected module is defective.

RF cables can be disconnected from the module output connectors; then, a power meter or spectrum analyzer can be connected directly to the module connector for power level or frequency measurements. Fabrication of a short coax adapter cable, terminated in a mating connector for the modules on one end and a BNC connector on the other, will facilitate connection of test equipment.

A problem in a power supply may cause many symptoms pointing to other areas, and should be checked when the symptom does not indicate a specific problem.

### 5.4.1 TROUBLESHOOTING HINTS

Following is a list of several typical symptoms, accompanied by the possible cause(s) or a troubleshooting procedure, it is assumed the instrument has been properly calibrated previously, and that a warm-up period will precede troubleshooting.
$\pm 18 \mathrm{~V}$ OUT OF CALIBRATION - If the $\pm 18 \mathrm{~V}$ supplies measure low, unplug modules until an overload is found.

INTERMITTENT OPERATION - Check for loose RF cables or loose modules. If none, check for defective module pin sockets.

INCORRECT HORIZONTAL OUTPUT - If horizontal output is incorrect, check module M101B.

INCORRECT SWEEP RATE - Check wiring to front-panel SWEEP TIME switch and M101B.

FREQUENCY UNSTABLE (JITTER) - Check all modules for loose hold-down screws, especially modules M102A and M103A. Operating the unit in a strong magnetic field, such as setting on top of, or adjacent to, another instrument containing a large power transformer can produce 60 Hz hum modulation.

If all bands are unstable, check for excessive ripple on power supplies.

NO RF SWEEP . Check all bands. If none sweep, try the other sweep mode. If still none sweep, check the rear-panel PROGRAMMING plug.

If only one band has no RF sweep, check the appropriate sweep drive signal. If correct, the trouble is probably in the Sweep Oscillator.

RF OUTPUT NOT FLAT - Most common cause is the external RF detector being defective. Another is the monitor diode located in the MA111 module. This is a point contact diode and can be damaged if the RF output is momentarily connected to a B+ voltage. A good monitor diode will produce a negative detected voltage (at pin 13 of M104A) approximately twice the amplitude of the external detector. For example, at an RF output of +10 dBm , an external RF detector will read approximately 0.8 V . The internal monitor will read approximately -1.6 V .

NO RF OUTPUT - All bands - Defective Attenuator or RF cables connecting to the input or output of the Attenuator. Single band only - if only one band does not work, check for the switched $B$ - voltage at the appropriate module socket as shown on the instrument Wiring Diagram.

## MARKER PROBLEMS

To isolate the cause of a marker problem when the symptom does not clearly indicate a specific circuit or component, first check the sweep sample output at the MA111 Sweep Sample Out connector. It should be a detected signal of between 30 and 50 mV . If the proper sweep sample signal is not present, it indicates that the trouble is in the MA111.

Next, connect the detector in place of the Terminating Plug, P102. A signal at this point indicates all jumper cables and RF jacks on the M6 modules are intact. Check for the birdy output at pin 3 of the marker module. A 10 to 15 mV peak-to-peak birdy is sufficient to drive the M105 module and indicates the M6 module is operating properly. With the 10 mV peak-to-peak birdy present at the input of
the M105 (pins 5, 6, 7, 8, 9), a 20 V peak-to-peak signal will be produced at the output (pin 1). This indicates proper operation of the M105. This output signal at pin 1 is controllable in width by the front-panel MARKER WIDTH control. The signal is now routed through the front-panel MARKER SIZE control to the front-panel VERT OUT connector. A 4 V peak-to-peak signal is normally at this point when the front-panel MARKER SIZE control is set to maximum. A common marker problem occurs when one of the interconnecting cables between the M6 modules is loose. This causes a notch in the sweep sample input to the module, causing uneven harmonics or weak output.

### 5.5 FIELD INSTALLATION OF OPTIONS

All options available on the Model 2002A can be field installed as described below. In each case, refer to Figures 5-22 and 5-23 for locations of sockets, cables, etc. In each case, the top and bottom covers of the instrument must be removed. (For Option B5, only the top cover need be removed.)

### 5.5.1 OPTIONS A1 and A2

Install Options A1 and A2 as follows:

1. Plug the M6 module into the appropriate socket and install the hold-down screw through the instrument chassis.
2. Connect the cable supplied to one of the connectors on top of the module.
3. Remove the Terminating Plug from the M6C or other marker module and install it on the open connector of the M6.
4. Connect the open end of the cable to the connector on which the Terminating Plug had been installed.
5. Replace the blank front-panel pushbutton corresponding to the marker socket used (see Schematic 1B) with the engraved button supplied.
6. Using the test set-up shown in Figure 4-1 (BAND switch set to 2 for harmonic markers, to the appropriate band for single-frequency markers), adjust the Marker Size control, accessible through the instrument chassis, for the correct operating level (see Section 5.3.6).

## NOTE

If an M66H Dual Harmonic Marker module is to be installed, it will occupy two marker sockets.

### 5.5.2 OPTION A3

Install Option A3 as follows:

1. Plug the M106 Deluxe Harmonic marker module into the appropriate socket and install the hold-down screw through the instrument chassis.
2. Remove connection cable W5 from the M6C External Marker module and install it on the M106 connector further from the M6C.
3. Connect the cable supplied to the open connectors on the M6C and the M106.
4. Remove the "OPTION NOT INSTALLED" knob from the instrument front panel, and install the new knob supplied.
5. Using the test set-up shown in Figure 4-1 (BAND switch set to 4), adjust the four Marker Size adjustments, accessible through the instrument chassis, for the correct operating levels, i.e. saturated markers (see Section 5.3.6).

### 5.5.3 OPTION B4

Install Option B4 as follows:

1. Remove the binding posts from the mounting bracket of the Pen Lift assembly.
2. Remove the option plate from the instrument rear panel, and remove the two plug buttons from the holes marked "PEN LIFT".
3. Place the mounting bracket against the option plate such that the bracket holes line up with the PEN LIFT holes, and the component side of the bracket will face the instrument power transformer when the option plate is reinstalled.
4. Insert the binding posts through the option plate and mounting bracket from the outside, and secure each using, in order, the shoulder washer, lock washer, and nut provided.
5. Solder each binding post to the wire immediately adjacent to it.
6. Re-install the option plate on the instrument rear panei.
7. Solder the gray wire to pin 10 of the M106 socket.
8. Solder the orange wire to pin 9 of the M106 socket.

### 5.5.4 OPTION B5

Install Option B5 as follows:

1. Remove the Terminating Plug from the M6C or other marker module and connect the Aux RF Out cable to the module connector.
2. Remove the plug button from the rear-panel hole marked 'AUX RF OUT'".
3. Unscrew the BNC connector body, lockwasher, and backing nut from the Aux RF Out cable.
4. Insert the BNC connector body through the rear-panel AUX RF OUT hole and secure it with the backing nut and lockwasher.
5. Screw the cable into the connector body.
6. Connect the 50 ohm terminator to the BNC connector. When Option B5 is in use, the terminator is removed. When the option is not in use, the terminator must be connected.


Figure 5-22. Top View


Figure 5-23. Bottom View

### 6.1 INTRODUCTION

This section contains lists of all replaceable parts for the instrument.

For an assembly containing one or more subassemblies, the assembly list appears first, and is followed by the subassembly lists.

The lists appear in the following order.

| PARTS LIST | ASSEMBLY |
| :--- | :--- |
| $1010-00-0141$ | 2002A |
| $1111-00-0083$ | CHASSIS |
| $1118-00-0040$ | REAR PANEL |
| $1219-00-0152$ | R.P. HARNESS |
| $1118-00-0018$ | FRONT PANEL |
| $-1219-00-0150$ | F.P. SUB-ASSY PARTS |
| $1118-00-0029$ | HARNESS |
| $1115-00-0011$ | PEN LIFT |
| $1218-00-0250$ | DPS2A |
| $1219-00-0144$ | PC - DPS2A |
| $1114-00-0267$ | LINE CORD - DPS2A |
| $1114-00-0268$ | M101B |
| $1114-00-0269$ | M102A |
| $1114-00-0270$ | M103A |
| $1114-00-0137$ | M104A |
| $1114-00-0138$ | M105 |
| $1219-00-0055$ | M109 |
| $1219-00-0070$ | RF MIXER - M109 |
| $1114-00-0139$ | PRE-AMP - M109 |
| $1118-00-0014$ | M110 |
| $1218-00-1111$ | MA111 |
| $1218-00-1110$ | I/O NTWK - MA111 |
| $1218-00-1100$ | I/O NTWK - MA111 |
| $1114-00-0205$ | BIAS CKT - MA111 |
| $1114-00-0252$ | M121 |
| $1114-00-0251$ | M131 |
| $1114-00-0124$ | M132 |
| $1114-00-0050$ | M6C |
| $1114-00-0099$ | M6H-1 |
| $1114-00-0100$ | M6H-10 |
| $1114-00-0045$ | M6H-50 |
| $1114-00-0152$ | M6S-3 |
| $1218-00-1180$ | M106 |
|  | PC - M106 |
| 110 |  |

### 6.2 MANUFACTURERS CODE

The following code is used on the parts lists to identify the manufacturer.

| ABERV | NIAME. | CITY. | ST |
| :---: | :---: | :---: | :---: |
| $A-E$ | ALLEN-GRADLEY | MILWAUKEE | WI |
| $A-D$ | ANALQG DEVICES | CAMBRIDGE | MA |
| A-H | ARROW HART, INC. | KETTERING | OH |
| A-I | ALIAN INDUSTRIES | COLUMBUS | IN |
| $A-M$ | AMERICAN MAGIUETICS | CARTERVILLE | IL |
| $A-P$ | AMERICAN PLASTICRAFT CO. | CHICAGO | IL |
| ABAC | ABACUS PACKAGING CO. | CHICAGO | IL |
| $A C I$ | ADVAPVE COMPONEINTS, INC. | CENTERBROOK | CT |
| AER | AVX CERAMICS | MYRTLE BEACH | SC |
| AERTK | AERTECH INDUSTRIES | SUNNYVALE | CA |
| AHAM | AHAM CEMPANY | AZUSA | CA |
| AIN | ALPHA INDUSTRIES: INC. | WOBURN | MA |
| ALC | ALCO ELECTRONICS PRODUCTS | NORTH ANDOVER | ME |
| ALLPL | ALL PLASTICS, INC. | IND I ANAPOL IS | IN |
| AMD | ADVANCED MICRO DEVICES INC. | SUNNYVALE | $C A$ |
| AMD | ADUANCED MICRO DEVICES, INC. | SUNNYVALE | CA |
| AMELC | AMERICANU ELECTRIC CORDSETS | BENSENVILLE | IL |
| AMP | AMP, INC. | HARRISBURG | PA |
| $A P L$ | AMPHENOL CGNTUECTOR SYSTEMS | BROADVIEW | IL |
| $A P X$ | AYPEREX ELECTRONIC CORP. | SLATERSVILLE | RI |
| ARC | ARCO ELECTRIC PRODUCTS | SHELBYVILLE | IN |
| ARN | ARNOLD ENGINEER ING CO. | MARENGO | IL |
| ARW-M | ARROW-M CORP. | CARSON | CA |
| ASC | ASSCCIATED SPRING | BRISTOL | CT |
| ASE | AIRCO SPEER ELECTRONICS | ST. MARYS | PA |
| AT/IN | ATLANTIC INDIA RUBBER COMPANY | CHICAGO | IL |
| ATC | AMERICAIV TECHNICAL CERAMICS | HUNTINGTON STATION | NY |
| ATR | ATR COIL CO. | BLOOMINGTON | IN |
| AUGAT | AUGAT, INC. | ATTLEBORD | MA |
| AULT | AULT INC. | MINNEAPOLIS | MN |
| AVT | AVANTEK, INC. | SANTA CLARA | CA |
| AlvC | ALPHA WIRE | ELIZABETH | NJ |
| B-T | BEh-TEK, INC. | READING | PA |
| BEK | BECKMAN INSTRUMENTS, INC. | FULLERTON | CA |
| BEL | BELDEN CORP. | GENEVA | IL |
| BER | BERG ELECTRONICS | NEW CUMBERLAND | PA |
| BGH | BEECH GROVE HARDWARE | BEECH GROVE | IN |
| BORDN | RORDEN INC. | COLUMBUS | OH |
| BOU | BOURNS, INC. | RIVERSIDE | CA |
| BREZ | BREEZE CORPORATIOINS, INC. | UNION | NJ |
| BUCK | BUCLEYE STAMPING CO. | COLUMBUS | OH |
| BUD | BUD RADIO, INC. | WILLOUGHBY | OH |
| BURND | BURNDY CORP. | NORWALK | CT |
| BUE | BUSSMAN MFG. | ST. LOUIS | MO |
| BWC | BARON WIRE AND CABLE CORP. | NILES | IL |
| $C-D$ | CORTUELL DUBILIER ELECT. DIV. | NEWARK | NJ |
| $C-E$ | CLINTON ELECTRONICS | ROCKFORD | IL |
| $\mathrm{C}-\mathrm{H}$ | CUTLER-HAMMER, INC. | MILWAUKEE | WI |
| $\mathrm{C}-\mathrm{I}$ | COMPONENTS, INC. | BIDDEFORD | ME |
| $\mathrm{C}-\mathrm{J}$ | TRW/CINCH | ELK GROVE VILLAGE | IL |
| c-K | C \& K COITPONENTS, INC. | WATERTOWN | MA |
| C-L | CEITRALAE DIV. | MILWAUKEE | WI |
| C-W | C-W INDUSTRIES | WARMINSTER | PA |
| CAI | CUSTOH ACCESSORIES, INC. | SKDKIE | IL |
| CAM | CAMBIDN | CAMBRIDGE | MA |
| CAR | CARLING ELECTRIC, INC. | WEST HARTFORD | CT |


| ABBRV | NAME | C | ST |
| :---: | :---: | :---: | :---: |
| CCM | CORCOM, INC. | CHICAGO | IL |
| CDC | COMPONENT DEVELOPMENT CORP. | CARSON | CA |
| CECD | CENTRAL COIL CO. | BRAZIL | IN |
| CGW | CORNING GLASS WORKS | CORNING | NY |
| CHE | CHERRY ELECTRICAL PRODUCTS | WAUKEGAN | IL |
| CHOM | CHOMERICS INC. | WOBURN | MA |
| CHRY | CHRYSLER CORP. | DETROIT | MI |
| CIMCD | CIMCO WIRE AND CABLE INC. | ALLENDALE | NJ |
| CKI | CTS KNIGHTS, INC. | SANDWICH | IL |
| CLA | CLAIREX CORP. | MT. VERNON | NY |
| CLAR | CLAROSTAT MFG. CO | DOVER | NH |
| CLFX | COLE-FLEX CORP. | BABYLON | NY |
| CPKG | CREATIVE PACKAGING DIV. | INDI ANAPOL IS | IN |
| CTS | CHICAGO TELEPHONE SYSTEMS | CHICAGO | IL |
| CTS-E | CTS OF ELKHART | ELKHART | IN |
| CTSBR | CTS OF BERNE | BERNE | IN |
| CTSBV | CTS OF BRGWNSVILLE | BROWNSVILLE | TX |
| DAL | DALE TECHNCLOGY CORP. | HARTSDALE | WY |
| DAV | HARRY DAVIES MOLDING CO. | CHICAGO | IL |
| DAYTN | DAYTON ELECTRIC CO. | CHICAGO | IL |
| DEL | DELEVAIV DIV. | EAST AURIRA | NY |
| DEN | DENNISCN MFG. CO. | FRAMINGHAM | MA |
| DEW | DEWIRE FABRICATINE CORP. | LOWELL | 11A |
| DILEC | DILECTRON | MONROVIA | CA |
| DID | DIODES, INC. | CHATSWORTH | CA |
| DRA | DRAKE MANUFACTURIVG CO. | HARWDOD HEIGHTS | IL |
| E-C | ELECTRONIC CRYSTALS | KAVSAS CITY | Mo |
| E-M | ELECTRA/MIDLAFD CORP. | MINJERAL WELLS | TX |
| ECMC | ELECTRI-CORD MFG. CO. IVC. | WESTFIELD | PA |
| ELCO | ELCD INDUSTRIES | ROCKFORD | IL |
| ELFX | ELECTRO-FLEX HEAT INC. | BLOOMFIELD | CT |
| EMRON |  |  | 5 |
| EPITK | EPITEK ELECTRONICS | MANATA, ONT. , CAN. | ** |
| ETP | ERIE TECHNOLDGICAL FRQDUCTS | ERIE | PA |
| EXAR | EXAR INTEGRATED SYSTEMS | SUNFVVALE | CA |
| F-K | THERMWELL PRODUCTS, INC. | FRAMINGHAM | MA |
| F-S | FEDERAL SCREW | CHICAGO | IL |
| FAN | FANCOURT \& CO. | GREENSBORO | NC |
| FASTX | FASTEX DIV., ILL. TOOL WORKS | DES PLAINES | IL |
| FCD | FAIRCHILD | MOUNTAIN VIEW | CA |
| FRK | FRAKO | FRANKFORT, GER. | ** |
| FRTE | FAIR RITE PRODUCTS CORP. | WALLKILL | NY |
| FRXC | FERROXCUBE DIVISION | SAUGERTIES | NY |
| G-E | GENERAL ELECTRIC | INDI ANAPDLIS | IN |
| G-H | GRAYHILL, INC. | LA GRANGE | IL |
| G-I | GEN'L INSTRUMENT SEMICONDUCTOR | HICKSUILLE | NY |
| G-T | GRAND TRAFSGFORMERS | GRAND HAVEN | MI |
| GAL | GALILED ELECTRO-OPTICS | CARMEL | IN |
| GATES | GATES ERERGY PROD. | DENVER | CO |
| GBN | GILBERT ENGINEERING CD. INC. | PHDENIX | AZ |
| GNATR | GENERAL ATRONICS CORP. | PHILADELPHIA | PA |
| GOU | GOULD, INC. | ST. PAUL | MN |
| GRIES | GRIES REPRODUCER | NEW ROCHELLE | NY |
| GRIP | GRIPMASTER CD. | MARLBORO | NJ |
| GUDL | GUDEBRDD BROS. SILK CO. | CHICAGO | IL |
| H-P | HEWLETT-PACKARD | INDIANAPOLIS | IN |



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HARTW HARTWELL CORP.
HEL HELIPQT
HEY HEYIIAN IIFG. CQ.
HHS HERTIATN H. SMITH, INC.
HIT HITACHI AMERICA. LTD.
HOLGW HOLLIVGSWORTH SLDRLS TERM.
HOLUB HOLUB DISTRIBUTING CO.
HED HARRIS CORP. SEMICDR. DIV.
HUD HUDSON TOOL & DIE CO.
HY/PL HYDRO PLASTICS INC.
HYT HYTRONICS
ICI ILLIHOIS CAPACITOR INC.
IERG IHT'L ELEC. RESEARCH CORP.
INDEG INOUSTRIAL EIECTRORIC HDWR.
INT INTERSIL, INC.
INWES INTERNATIGNAL WERBING
IRG INTERNATIDNAL RESIGTANCE CO.
IREC IHTTL REETIFIER CORP.
ITT IHT'LL TELEFHONE & TELEGPAPH
GAN JATM HARDNARE TIFS. CD.
JEF JEFFERS
JEFWC JEFFERSON WIRE AND CABLE
UEW JE:HELL ELECTRICAL INSTRUMENTS
UHSN JIHANSON NFG. CGRP.
JON E.F. JOHRSON CO.
UUDD UUDD WIRE DIV. ECC
K-L KERRIGAN LEWIS MFG.
N-S K z S ENGINEERING CO.
KEENE KEELIE CORP.
KEEN KEMTRON ELECTRON PRODLICTS
KEY KEYETONE ELECTRONIC CGRP.
KID FIDCO INC.
KIN NINGS ELECTRUNICS
ASTR KESTER SOLDER DIV.
KSW KSW ELECTRONICS
KUL KULKA ELECTRIC CORP.
BAURN LFUNEN HFO CO.
LEYSE LEYGE ALUHINUM CO.
LIT LITTELFUSE, INC.
LRC LRC ELECTRONICS: INC.
M-A MICROWAVE ASSOCIATES
H-D FILLER DIAL * NAMEPLATE CO.
M-E MEPEO ELECTRA. INC.
MO ILLUMIUATEO FRODUCTS ITC.
H-F MICRO PLASTICS INC.
MAL MGLLERY COHTROLS CO.
MAND MANDEX
MARQ J. z J. MARQUARDT
MDC MAIDA DEVELDPMENT CO.
MILN MILLEN MFG. CQ.
MILGP MILITARY GPECIFICATIORA
MINDR MINGR RUBBER CO.
MITEK MITEEK
MLRJW J.W. MILLEER
MMM JM COMPANY
MNO MONSARTD COMIT. PROD. DIV.
```

| $A B E R V$ | WArME | C | ST |
| :---: | :---: | :---: | :---: |
| MOL | MTLEX PROLUCTS | LISLE | IL |
| MORAD | MGRGAN ADHESTVES | STOW | OH |
| MOT | MOTOROLA SEMI. PROD. DIV. | INDIATVAPOLIS | IN |
| MRO | HICRO SWITCH DIV. | FREEPIRT | IL |
| MSN | MICROSOTICS DIV. | WEYMIOUTH | MA |
| MSP | MICRO SEMICONOUCTOR CORP. | SANTA ANA | CA |
| Hhs | HAQRET WITE SUPPLY CO. | CHATSWORTH | CA |
| MYERS | MYERS SPRIVAO CO. | LOGANSPORT | IN |
| N-T | GATIONAL TEL-TRONICS | LAREDO | TX |
| NAT | IMATIORAL SEMICONDUCTOR CGRP. | SAITTA CLARA | $C A$ |
| NEC | HIPPON ELECTRIC CO. | TOKYD, JAPAN: | * |
| MEL | NATIDNAL ETUGINEERING LABS | INDIANAPOLIS | IN |
| NEW | HEWARM ELECTRONICS | INDIANAPOLIS | IN |
| NPC | WUCLEOUTC PRODUETS CO. | CANOGA PARK | CA |
| MYLG | HYLOMATIC | MORR ISVILLE | PA |
| D-G | GPTI-GAGE INC. | DAYTON | OH |
| D-S | ORFI SPECTRA INC. | FARMINGTON | MI |
| DAK | OAK INDUSTRIES INC. | CRYSTAL LAKE | IL |
| OHM | OHMITE !IFG. CO. | GKOKIE | IL |
| DrAEGA | [MESA WIFE \& CADLE | HARLEYSVILLE | PA |
| DPTRN | GPTRON ITG: | CARROLL TON | TX |
| $P-B$ | POTTER AND BRUMFIELD | PRINCETON | IN |
| $P-C$ | PONER COMPCNEITS | WOODLAKD HILLS | CA |
| $p-K$ | PARKER KALON CORP. | CLIFTON | MJ |
| $P-T$ | PENN TUBE PLASTISS CO. | CLIFTON HEIGHTS | PA |
| P-U | FROUECTS UNLIMITED INC. | DAYTON | OH |
| POLFH | PQLYPHASE INSTR. CO. | BRIDGEPORT | PA |
| PAM | PAMOTOR DIV. | BURL INGAME | CA |
| PAIM | PAMOTOR DIV. | BURLINGAME | $C A$ |
| PAND | PAIJLUIT CERP. | TINLEY PARK | IL |
| PARA | PARAPETRIC ITUDUSTRIES | NORTHFIELD | IL |
| $P G C$ | PATUEL CQMPGNETTS CGRP. | BERKELEY | CA |
| PEC | PACIFIC ELECTRICORD CO. | GARDENA | CA |
| PHC | PHILADELPHIA HANOLE CO. | CAMDEN | NJ |
| PIC | PIHER INTERINATIONAL CGRP. | ARLINGTON HEIGHTS | IL |
| PLSSY | PLESSEY ENG. | SCHILLER PARK | IL |
| PMCL | PERMACEL DIV. | NEW ERUNSWICK | N. |
| PMI | PRESISION MOHOLITHICS INC. | SANTA CLARA | CA |
| POM | FOMONA ELECTRONICS CO., IVC. | POMONA | $C A$ |
| PRMD | PYRAMID INDUSTPIES, INC. | PHOENIX | $A Z$ |
| PRSN | PRECISICN TURE CO., INC | NORTH WALES | PA |
| PTN | PENH TRAH CORP. | BELLEFONT | PA |
| PYRD | PYRCFILIT CORP. | WHIPPANY | NY |
| PYTT | FYTTRONICS IHDUSTRIES, INC. | MONTGOMERYVILLE | PA |
| $Q-C$ | GUALITY COMPCNENTS | ST. MARYS | PA |
| $\mathrm{R}-\mathrm{N}$ | ROEINSON-MUGENT | NEW ALSATVY | IN |
| RAY | RAYTHEON | INDIANAFOLIS | IN |
| RCA | RCA | CAIMDEN | NW |
| PEL | RELIAMCE MICA CO. | BROOKLYN | HY |
| RGR | FOQERS CORP. | CHANDLER | $A Z$ |
| RICH | RICHCO PLASTIC CO. | CHICAGO | IL |
| RICHM | RICHARDS METAL PRODUCTS | WOLCOTT | CT |
| RMC | RADID MATERIALS CORF. | CHICAGO | IL |
| RMF | RMF PRODUCTS INC. | Batavia | IL |
| ROGAN | ROSAH CCRP | NORTHBROOK | IL |
| $S-C$ | SPECIALTY COHNEGTOR | INDIANAPOLIS | IN |T

WOL MGLEX PRODUCTE LISLE IL
MORAD FORGAR ADHESTVES STOW OH
MOT FOTOROLA EEMI. PROD. DIV.
MRO FICRO GWITCH DIV.
MSN MICROSOIVICS DIV.
MSP MICRO SEMICONOUCTOR CORP.
HhS HAORET WIIRE SUPPLY CD.
MYERS MYERS SPRIFUG CO.
NAT ISATIONAL GEMICONDUCTOR CORP.
NEG HIPPON ELEGTRIC CO.
NEL NATIONAL EHGINEERING LABG
NEW HEWARK ELECTRONTCS
NPG WUKLEONIC PRODUETS CO.
NYLG NYLOMATIC
D-G GPTI-GAGE INC.
D-S DFHI SPECTRA IHC.
DAK DAK INDUSTRIES INC.
OHM GHMITE !HFg. CO.
DHEGA [MEGA NIFE \& CADLE
DPTRN GPTRON IUU*
PGTIER AMD BRUMFIELD
poner campenemts
Mat

P-U FRONECTS UNLINITED INC.
POLFH POLYPHASE INSTR. CO.
PAM PAKITOR DIV.
PAM PAMOTOR DIV.
PAND PAISLUIT CGRP.
PARA PARAFETRIC ITUDUSTRIES
PGC PATUEL COMPGNETTG CORP.
PEG PACIFIC ELEGTRIGORD CQ.
PHC PHILADELPHIA HANOLE CO.
PIC PIHER INTEPMATIGNAL CURP
PLSSY PLEGSEY ENG.
PMI PRESISION MOHOLITHICE INC.
POM FOMONA ELECTRONICS CO., INC.
FRMD PYRAMID INDUSTRIES, INC.
PRGN PRECIGICN TURE CO. , INC
PTN PENA TRAN CORP.
PYRO PYRCFILIM CORP.
PYTT FYTTRONICE IHDUSTRIES, INC.
Q-C GUALITY COMPONENTS
R-N ROBINSON-NUGENT
RAY RAYTHEON
RCA RCA
REL RELIATUCE MICA CO.
RGR FDGERS CORP.
RICH RICHCO PLASTIG CO.
RICHM RICHARDS METAL PRODUCTS

ROGAN ROGAH CORP
S-C SPECIALTY CONEGTOR

| ABBPU | NAME. | CITY. | $5 T$ |
| :---: | :---: | :---: | :---: |
| s-6 | GTANDAFD GRIESBY | AURORA | IL. |
| S-5 | SHITCHCRAFT, ITE. | CHICAOD | IL. |
| S-S | SERUICE SUPPLY | ITOIANAPDLIS | IN |
| S-T | GARKES TAPLIAP | BLOUMINGTON | IN |
| GCDE | SCATBE DIVISION | EL MOISTE | $C A$ |
| Scc | STACHPGLE CARPOL CO. | ET. MARYS | PA |
| ECx | GJLICOHITX INC. | garta clara | CA |
| GEAST | SEASTRCM HFG. 6. | QLENDALE | $C A$ |
| SECR | SECOR IUC. | WEGTWOOD | HJ |
| CEL | GEALECTRO CORP. | MAMARONECK | NY |
| SEM | SEMTECH | NEWBURY PARK | $C A$ |
| SEMTX | SEMTEX | DAYTON | OH |
| SGM | SIGTA INSTRUTENTS | BRA INTREE | MA |
| SHAM | SHAMROCK PLASTICE \& RUBSER CO. | INDI ANAPOLIS | IN |
| SIEM | SIEMENS | ISELIN | HJJ |
| Slo | SIGRETISS CORPORATION | SUNNYVALE | CA |
| SLT | EGLITRON/HICROWAVE DIV. | PORT SALERNO | FL |
| SHTC | CAITTEC IINC. | NEN ALBATVY | IN |
| SOUTH | SOUTHCO FASTEIERS | LESTER | PA |
| SPE | SPECTROL | DAYTON | OH |
| SPEC | SPECTRUM CONTROL INC. | FAIRUIEW | PA |
| EPR | SPRAGUE ELECTRIC CO. | IMDIANAPCLIS | IN |
| EPST | GPECTRA-STRIP | GARDEN GROVE | $C A$ |
| 95s | SULID STATE SCIENTIFIC | MONTGOMERYVILLE | PA |
| STDPS | STANDARD PRESSED STEEL | JEEWKINTOUN | PA |
| ETR | GTETTNER TRUSH CO. | CAZENOVIA | ITY |
| STSA | STEEL SALES | IND I ANAPCLIS | IN |
| SYL | GTE SYLVANIA | WAL THAM1 | MA |
| SYS | SYSCON INTERNATIONAL, INC. | SOUTH BEND | IN |
| T-I | TEXAS INSTRUMENTS | DALLAS | TX |
| TCPL | TACONIC PLASTIC | PETERSBURG | NY |
| TEK | TEKTRONIX | INDIANAPOLIS | IN |
| TEKA | TEKA PRODUCTS INC. | COLLEGE POINT | WY |
| TELE | TELETYFE CORP. | ELK GROVE VILLAgE | IL |
| THR | THERMALLOY CO. | DALLAS | TX |
| TIMES | TIMES WIRE AND CABLE | CITVCINNA I | OH |
| TIN | TINTERTIAN PRDDUCTS, IKY. | CLEVELAIND | OH |
| TKN | TECHNICAL INIRE | CRAWFORD | NJ |
| TLNC | TELGNIC ALTAIR | LAGUNA BEACH | CA |
| TORCO | TOR CORP. | VAN NUYS | CA |
| TR-UT | TRIAD-UTRAD DIV. | HUNTINGTON | IN |
| TRU | WALDES TRUARC | LONG ISLAND CITY | NY |
| TRW | TRW CAPACITOR DIV. | OGALLALA | NB |
| TVL | TEL-VISION LABS | WAUCONDA | IL |
| U-C | UNIVERSAL COHTPONENTS | LOS ANEELES | $C A$ |
| UNCAR | UNION CARBIDE COHPONENTS | GREENVILLE | SC |
| UNIC | UNICORP | ORANGE | NJ |
| UNIT | UNITRODE CORP. | WA TERTOWN | HA |
| USECO | USECO DIV. | VAIN NUYS | $C A$ |
| UTK | UNITRACK DIV. | UPPER DARBY | PA |
| VAC | UACTEC INC. | MARYLAND HEIGHTS | MO |
| VACO | VACO PRODUCTS CO. | NORTHBROOK | IL |
| UAR | VARADYIEE CAPACITOR DIV. | SANTA MONICA | $C A$ |
| VARIL | VARI-L CO. | DENVER | CO |
| VELCR | VELCRO USA INC | NEW YORK | NY |
| VLIER | VLIER ENGINEERING CORP. | BURBANK | CA |

ADRRU HAME. ........................... CITY. ..... ST
VONGT VOWTEGUT HARDWARE INDI ANAPOLIS ..... IN
VRN VERISTRGN COFP. GREAT NECK ..... NY
VRE VERNITRON CORF. GREAT NECK ..... ny
H-E WELLS ELECTROHISS
W-Y WAVETEK INOIARA INC.
WAG WAGTUER ELECTRIC CORP.
WECK WECHESEEF CO. INC.
WHFLD WAKEFIELD EUGTUEERIHQ
WHE! WEINSCHEL ENGURERING
WGE WAVETEK
SER WAVETER
ZEN ZENITH RADID GORF.
ZERO ZERD MANUFACTURIVQ OO.
ZIE ZIERICA FFE. COPF.
ZPT ZIPPERTUBING, ©O.


| REFERENCE DESİNATORS | part description | ORIG-mFgr-PART-KO | MFgr | WAVETEK No. | aty |
| :---: | :---: | :---: | :---: | :---: | :---: |
| P1 <br> P5 <br> W1 W2 <br> W3 <br> W4 <br> W5 <br> W6 <br> HH1 | PROG PLUG, A529-004 SMC TERM, 50 A500-267 Cable Assy, 2-1/2 in cable assy, 4-1/2in CAble ASSy, 2-3/8 in CABLE ASSY, 10-1/4 IN CABLE ASSY, 12 in harness 2002A-A, b, C | A529-004 <br> A500-267 <br> wx2002-w1 <br> wx2002-w3 <br> Wx2002A-W4-WNSL <br> wx3000-200-w21 <br> wx2002-wb <br> 1219-00-0150 | ${ }^{\omega}-1$ <br> w-I <br> w-I <br> W-I <br> w-I <br> w-I <br> W-I <br> w-I | 1118-00-0012 1118-00-0007 1217-00-0024 1217-90-0016 1217-90-0038 1217-00-0102 1217-80-0022 1219-00-0150 | $1$ |
| Wavetek PARTS LIST | $\operatorname{SWP}_{\text {Tifle }}^{\text {GEN, }}$, 2002A | ASSEMBLY $1010-00$ <br> page: 2 |  |  | $\stackrel{\text { REV }}{\text { A }}$ |







| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C4 | CAP, CER, 15PF, 1KV | 10TCC-Q15 | SPR | 1510-10-0150 | 1 |
| CR2 CR3 | DIODE | IN4 148 | FCD | 4807-01-0914 | 2 |
| CR4 CR5 CR6 CR7 CR8 CRg CR10 CR11 | DIODE | IN4004 | P-C | 4806-01-4004 | 8 |
| CR12 | DIODE | IN34A | HIT | 4807-01-0034 | 1 |
| P1 | PLUG,36-PIN | 03-06-236? | MOL | 2113-04-0005 | 1 |
| NONE | TERMINAL, MALE | 1854 | MOL | 2113-05-0002 | 6 |
| P20 1 | PLUG | 19-09-2042 | MOL | 2113-26-0001 | 1 |
| NONE | TERMINAL, MALE | 02-09-2118 | MOL | 2113-09-0004 | 4 |
| R4 | RES, MF, $1 / 8 \mathrm{~W}, 1 \%$, 10 K | MF55K10K | ASE | 4701-03-1002 | 1 |
| R5 | RES, MF , 1/8W, 1\%, 40.2 K | MF 55K-40.2K | ASE | 4701-03-4022 | 1 |
| R6 | RES , C, $1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{~K}$ | CF $1 / 4-47 \mathrm{~K}$ | ASE | 4700-15-4702 | 1 |
| R7 R8 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ | CF $1 / 4-10 \mathrm{~K}$ | ASE | 4700-15-1002 | 2 |
| R9 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 43 \mathrm{~K}$ | CF-1/4-43K | ASE | 4700-15-4302 | 1 |
| R10 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 27 \mathrm{~K}$ | CF1/4-27K | ASE | 4700-15-2702 | 1 |
| R11 | POT, 50 K | $3605503 B$ | CTS | 4610-00-1503 | 1 |
| R12 | RES, MF, 1/8W, 1\%,47.5K | MF5 5K-47.5K | ASE | 4701-03-4752 | 1 |
| R13 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 470 \mathrm{~K}$ | CF $1 / 4-470 \mathrm{~K}$ | ASE | 4700-15-4703 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | SUB-ASSY PARTS | ASSEMBL <br> PAGE 1 |  |  | REV |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NE. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $J 1$ | RECEPTACLE,36-PIN | 03-06-1361 | MOL | 2113-03-0004 | 1 |
| NONE | TERMINAL, FEMALE MCOOO-018 | 02-06-1131 | MOL | 2113-05-6001 | 23 |
| J12 | HSG, MINI-LATCH, 1OPIN MCOOO-130 | 65039-027 | BER | 2113-10-0010 | 1 |
| NONE | PLUG, POLARIZING MCOOO-117 | 65307-001 | BER | 2113-23-0001 | 3 |
| NONE | $\begin{aligned} & \text { TERM, MINI-PU } \\ & \text { MCOOO-092 } \end{aligned}$ | 47439 | BEP | 2113-20-0001 | 19 |
| 32 | JACK, FEMALE, 9-CKT MCOOO-067 | 09-50-3091 | MOL | 2113-06-0001 | 1 |
| NONE | CONTACT MCOOO-068 | 08-50-0107 | MOL | 2113-07-0001 | 8 |
| U3 | $\begin{aligned} & \text { HSG, MINI-LATCH, 5-PIN } \\ & \text { MCOOO-115 } \end{aligned}$ | 65039-032 | BER | 2113-10-0001 | 1 |
| 14.84 | HSG, MINI-i_ATCH, S-PIN MCOOO-112 | 65039-031 | BER | 2113-10-0002 | 2 |
| NONE | TERM. MALE, MCOOO-116 | 48:16 | BER | 2113-22-000: | 6 |
| NONE | TERM, FEMALE MCOOO-042 | 02-06-1103 | MOL | 2113-05-0004 | 1 |
| WAVETEK PARTS LIST | SS 2002A-A, B,C | $\begin{aligned} & \text { ASSEMBLY } \\ & 1219-00 \end{aligned}$ <br> PAGE: |  |  | REV |







| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFG | -PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 |  | $\begin{aligned} & \text { TERM, FEMALE } \\ & \text { MCOOO-136 } \end{aligned}$ | 02-09-1118 |  | MOL | 2113-09-0003 | 4 |
| P202 |  | CORD SET, 18/3SVT, 6FT GRY, MLD. CAP, UL-APPRV | 17237SVT |  | BEL | 6011-80-0001 | 1 |
| WAVETEK PARTS LIST | $\begin{aligned} & \text { TITLE } \\ & \text { LINE CORD ASSEMBLY } \end{aligned}$ |  |  | $\begin{aligned} & \text { ASSEMBLY } \\ & 1219-00 \end{aligned}$ <br> page: | ASSEMBLY NO.$1219-00-0144$ |  | $\begin{array}{r} \text { REV } \\ \mathrm{B} \end{array}$ |


| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MF | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{lllll} \text { C01 } & \text { c02 } & \text { c03 } & \text { c04 } & \text { c05 } \\ \text { C06 } & \text { c07 } & \text { c08 } & \text { C18 } & \text { C19 } \\ \text { C20 } & \text { c21 } & \text { c22 } & \text { c23 } & \end{array}$ |  | CAP,F.T., 6. BPF CF102-R68 | FA5C-68 | 1510-30-1689 | 14 |
| C09 |  | CAP, MYLAR, . 15MF, 100 V CP103-415 | WMF 1P 15 | 1510-60-2154 | 1 |
| C10 C26 |  | $\begin{aligned} & \text { CAP, CER,. OO5MF, } 1 \mathrm{KV} \\ & \text { CD102-250 } \end{aligned}$ | 5GA-D50 | 1510-10-1502 | 2 |
| C11 C12 |  | CAP, CER, . OO1MFD, 1KV CD102-210 | 5GAD 10 | 1510-10-1102 | 2 |
| C13 |  | CAP, CER, 470PF, 1 KV CD102-147 | 60U471M | 1510-10-1471 | 1 |
| C14 C 17 |  | CAP, ELECT, 1MF, 25 V CE120-001 | 162D105 | 1510-21-7010 | 2 |
| C15 |  | CAP, CER, . $01 \mathrm{MF}, 100 \mathrm{~V}$ CD103-310 | 68 U 103 M | 1510-10-2103 | 1 |
| C16 |  | CAP, CER, 1OPF, 1KV CD101-010 | 10TCC-Q | 1510-10-0100 | 1 |
| C24 C25 |  | $\begin{aligned} & \text { CAP,F.T., 47OPF } \\ & \text { CF101-147 } \end{aligned}$ | FASC-47 | 1510-30-0471 | 2 |
| CRO1 CRO3 |  | DIODE DROOO-001 | 1 N4004 | 4806-01-4004 | 2 |
| CRO2 CRO4 CRO5 CRO6 <br> CRO7 CRO8 CRO9 CR10 <br> CR11 CR12 CR13 CR14 <br> CR15 CR17 CR18 CR19 |  | DIODE DG109-140 | 1N4148 | 4807-01-0914 | 18 |
| WAVETEK PARTS LIST | TITLE SWEEP | RATE, M101B |  |  |  |




| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MF | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R21 |  | $\begin{aligned} & \text { RES, MF, } 1 / 8 \mathrm{~W}, 1 \%, 56.2 \mathrm{~K} \\ & \text { RF213-562 } \end{aligned}$ | MF55K-5 | ASE | 4701-03-5622 | 1 |
| R22 |  | $\begin{aligned} & \text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 4.7 \mathrm{M} \\ & \text { RC } 103-547 \end{aligned}$ | CB4755 | A-B | 4700-15-4704 | 1 |
| R26 |  | RES, C, 1/4W, 5\%, 56K RC 103-356 | CF1/4-5 | ASE | 4700-15-5602 | 1 |
| R30 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 33 \mathrm{~K}$ RC 103-333 | CF1/4-3 | ASE | 4700-15-3302 | 1 |
| R31 |  | RES, C, 1/4W, 5\%, 22 RC103-022 | CF1/4-2 | ASE | 4700-15-2209 | 1 |
| R33 |  | RES, C, 1/4W, 5\%, 68K RC 103-368 | CF1/4-6 | ASE | 4700-15-6802 | 1 |
| R34 R42 |  | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 2.7 \mathrm{~K} \\ & \text { RC103-227 } \end{aligned}$ | CF1/4-2 | ASE | 4700-15-2701 | 2 |
| R35 R50 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{M}$ RC103-510 | CF1/4-1 | ASE | 4700-15-1004 | 2 |
| R37 |  | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 8.2 \mathrm{~K} \\ & \text { RC } 103-282 \end{aligned}$ | CF1/4-8 | ASE | 4700-15-8201 | 1 |
| R39 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 680 \mathrm{~K}$ RC 103-468 | CF1/4-6 | ASE | 4700-15-6803 | 1 |
| R44 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC103-310 | CF1/4-1 | ASE | 4700-15-1002 | 1 |
| WAVETEK PARTS LIST | title SWEEP | RATE, M101B |  |  |  | $\begin{array}{r} \mathrm{REV} \\ \mathrm{~B} \end{array}$ |





| REFERENCE DESIGNATOR | PART DESCRIPTION | QRIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { CAP,F.T., } 6.8 P F \\ & \text { CF102-RG8 } \end{aligned}$ | FA5C-6892 | A-B | 1510-30-1689 | 9 |
| $\operatorname{cog~Cil~}$ | $\begin{aligned} & \text { CAP, Q-C, } 2 . O P F, 10 \% \\ & \text { CG101-220 } \end{aligned}$ | QC-2. OPF | Q-C | 1510-40-0020 | 2 |
| C12 C13 | $\begin{aligned} & \text { CAP, CER }, .05 \mathrm{MF}, 100 \mathrm{~V} \\ & \text { CD103-350 } \end{aligned}$ | TG-550 | SPR | 1510-10-2503 | 2 |
| C14C15 | $\begin{aligned} & \text { CAP,F.T., 47OPF } \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | $A-B$ | 1510-30-0471 | 2 |
| CRO1 CRO2 CR03 CRO4 CRO5 CRO6 CRO7 CRO8 CRO9 CR10 CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 18 |
| IC01 IC02 ICO3 ICO4 | DUAL OP AMF, RAYTHEON IC000-027 | RC4558DN | RAY | 7000-45-5801 | 4 |
| R01 R02 R03 R04 R05 R06 | RES, MF, 1/8W, $1 \% 499$ RF211-499 | MF55K-499 | ASE | 4701-03-4990 | 6 |
| R07 R08 R09 R10 R45 R82 | POT, 20K, RP 130-320 | 89PR20K | BEK | 4610-00-2203 | 6 |
| R11 R12 R13 R14 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 330 \\ & \text { RC } 103-133 \end{aligned}$ | CF1/4-330 | ASE | 4700-15-3300 | 4 |
| R15 R16 R17 R18 R29 <br> R30 R31 R32 R46 R47 <br> R48 R49 R63 R64 R65 <br> R66     | RES, C, 1/4W, 5\%, 2. 2K RC 103-222 | CF1/4-2. 2 K | ASE | 4700-15-2201 | 16 |
| WAVETEK PARTS LIST | DRIVE, M103A | ASSEMBLY $1114-00$ <br> PAGE: |  |  | REV |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ```c01 co2 co3 co5 co7 C08 co9``` | CAP, CER, . O2UF, 50V | TG-520 | SPR | 1510-10-2203 | 7 |
| CO4 | CAP, TANT, . 47MF, 50 V CE113-447 | 935 | TRW | 1510-21-9470 | 1 |
| cob C10 | CAP, CER, 360PF, 1 KV CD102-136 | $60 \cup 361 \mathrm{M}$ | MDC | 1510-10-1361 | 2 |
| $\begin{array}{lllll} \text { C11 } & \text { C12 } & \text { C13 } & \text { C14 } & \text { C15 } \\ \text { C16 } & \text { C17 } & \text { C20 } & \text { C21 } & \text { C23 } \\ \text { C24 } & & & & \end{array}$ | $\begin{aligned} & \text { CAP,F.T., } 6.8 P F \\ & \text { CF102-R68 } \end{aligned}$ | FA5C-6892 | A-B | 1510-30-1689 | 11 |
| C18 C19 | $\begin{aligned} & \text { CAP, F.T. , 470PF } \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | A-B | 1510-30-0471 | 2 |
| CRO1 CRO2 CRO3 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 3 |
| ICO1 ICO3 | IC, 1C000-002 | N5741CV | SIG | 7000-57-4100 | 2 |
| 1-02 | DUAL OP AMP, RAYTHEON IC000-027 | RC4558DN | RAY | 7000-45-5801 | 1 |
| 001002 | TRANS QAO54-580 | 2N5458 | mat | 4901-05-4580 | 2 |
| Q03 G04 c05 | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 3 |
| Q06 | TRANS GAO54-610 | 2N5461 | MOT | 4901-05-4610 | 1 |
| R01 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 560 \mathrm{~K}$ RC 103-456 | CF $1 / 4-560 \mathrm{~K}$ | ASE | 4700-15-5603 | 1 |
| R02 R12 R23 | POT, 20K, RP 130-320 | 89PR20K | BEK | 4610-00-2203 | 3 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | ER, M104A | $\begin{aligned} & \text { ASSEMBLY } \\ & 1114-00 \end{aligned}$ <br> PAGE: |  |  | REV A |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-ND | MFER | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R18 | POT, 5K, RP 130-250 | 89PR5K | BEK | 4610-00-2502 | 1 |
| R19 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 330 \mathrm{~K}$ RC103-433 | CF1/4-330K | ASE | 4700-15-3303 | 1 |
| R20 R36 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC103-310 | CF1/4-10K | ASE | 4700-15-1002 | 2 |
| R21 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 200 \mathrm{~K}$ RC103-420 | CF1/4-200K | ASE | 4700-15-2003 | 1 |
| R24 | RES, C, 1/4W, 5\%, 270K RC 103-427 | CF1/4-270K | ASE | 4700-15-2703 | 1 |
| R30* | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 7.5 \mathrm{~K} \\ & \text { RC } 103-275 \end{aligned}$ | CF1/4-7.5K | ASE | 4700-15-7501 | 1 |
| R31 | RES, C, 1/4W, 5\%, 2. 2K RC103-222 | CF1/4-2. 2 K | ASE | 4700-15-2201 | 1 |
| R32 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 4.7 \mathrm{~K} \\ & \text { RC103-247 } \end{aligned}$ | CF1/4-4.7K | ASE | 4700-15-4701 | 1 |
| R33 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 6$. 8 K RC103-268 | CF 1/4-6.8K | ASE | 4700-15-6801 | 1 |
| R34 | $\text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 100$ RC103-110 | CF1/4-100 | ASE | 4700-15-1000 | 1 |
| R35 | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 68 K RC103-368 | CF 1/4-68K | ASE | 4700-15-6802 | 1 |
| R40 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 200$ | CF1/4-200 | ASE | 4700-15-2000 | 1 |
| WAVETEK PARTS LIST | TITLE <br> LEVELER, M104A | ASSEmbly $1114-00$ <br> page: |  |  | REV A |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK ND. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ```C01 co3 cos C16 C24 C26``` | $\begin{aligned} & \text { CAP, F.T., } 6 . \text { BPF } \\ & \text { CF102-R68 } \end{aligned}$ | FA5C-6892 | A-B | 1510-30-1689 | 6 |
| C02 c04 C06 C25 c27 | CAP, CER, . OO2MF, 1 KV CD102-220 | 5GAD20 | SPR | 1510-10-1202 | 5 |
| C07 C10 C22 C28 | $\text { CAP, CER , . O1MF, } 100 \mathrm{~V}$ CD103-310 | 68U103m | .1DC | 1510-10-2103 | 4 |
| c08 629 | CAP, TANT, 10MF, 25 V CE120-010 | 162D106×0025DD2 | SPR | 1510-21-7100 | 2 |
| c09 c23 | $\text { CAP, CER }, .001 \mathrm{MFD}, 1 \mathrm{KV}$ CD102-210 | 5GAD 10 | SPR | 1510-10-1102 | 2 |
| $\begin{array}{lllll} \text { C11 } \\ \text { C21 } \end{array}$ | CAP, CER, . O2UF, 50V | TG-S20 | SPR | 1510-10-2203 | 6 |
| C12 C13 C19 C20 | CAP, CER, 100PF, 1 KV CD102-110 | 60U101M | MDC | 1510-10-1101 | 4 |
| $\begin{array}{lllll} \text { C30 } & \text { c31 } & \text { c32 } & \text { c33 } & \text { c35 } \\ \text { C37 } & \text { c38 } \end{array}$ | $\begin{aligned} & \text { CAP, F.T., } 470 P F \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | A-B | 1510-30-0471 | 7 |
| C34 C36 | CAP, ELECT, 100MF, 25 V CE105-110 | TE1211 | SPR | 1510-20-4101 | 2 |
| CR1 | DIODE DROOO-001 | 1N4004 | P-C | 4806-01-4004 | 1 |
| IC1 IC2 | IC, 1C000-030 | LM318N | NAT | 7000-03-1800 | 2 |
| L1 L2 | $\begin{aligned} & \text { CHOKE, } 10 . \text { OMH, } 10 \% \\ & \text { LAOO5-010 } \end{aligned}$ | O8N100K | ASE | 1810-03-0100 | 2 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | DDER, M105 | ASSEMBLY $1114-00$ <br> PAGE: |  |  | $\begin{array}{r} \mathrm{REV} \\ \mathrm{C} \end{array}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-ND | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q01 Q02 003 Q04 005 | TRANS QAO50-880 | 2N5088 | MOT | 4901-05-0880 | 5 |
| Q06 008 Q15 017 | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 4 |
| $\begin{aligned} & \text { Q07 } 009010 \quad 011 \quad 012 \\ & \text { Q13 } \end{aligned}$ | TRANS QAO54-580 | 2N5458 | MOT | 4901-05-4580 | 6 |
| Q14 016 | TRANS QBOOO-009 | MPS3702 | MOT | 4902-03-7020 | 2 |
| R01 R04 R07 R47 R50 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 5.6 \mathrm{~K}$ RC 103-256 | CF1/4-5.6k | ASE | 4700-15-5601 | 5 |
| R02 R05 R08 R46 R48 | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 22K RC103-322 | CF1/422K | ASE | 4700-15-2202 | 5 |
| R03 R06 R09 R18 R34 R45 R49 | ```RES, C, 1/4W, 5%,270 RC103-127``` | CF 1/4-270 | ASE | 4700-15-2700 | 7 |
| R10 R41 | RES, C, 1/4W, 5\%, 4. 7K RC 103-247 | CF1/4-4.7K | ASE | 4700-15-4701 | 2 |
| R11 R12 R16 R36 R39 R40 | RES, C, $1 / 4 \mathrm{~W}, 10 \%, 10 \mathrm{M}$ RC 104-610 | CB1061 | $A-B$ | 4700-16-1005 | 6 |
| R13 R17 R19 R24 R25 R29 R33 R38 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC 103-310 | CF1/4-10K | ASE | 4700-15-1002 | 8 |
| R14 R21 R22 R27 R32 R37 | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 1K RC 103-210 | CFi/4-1K | ASE | 4700-15-1001 | 6 |
| R15 R35 | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 220K RC 103-422 | CF1/4220K | ASE | 4700-15-2203 | 2 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | DDER, M105 | ASSEMBL $1114-00$ <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{C} \end{array}$ |


| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R20 R23 R26 R31 |  | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 680$ RC 103-168 | CF1/4-680 | ASE | 4700-15-6800 | 4 |
| R28 |  | RES, C, 1/4W, 5\%, 100K RC103-410 | CF1/4-100K | ASE | 4700-15-1003 | 1 |
| R30 |  | $\begin{aligned} & \text { POT, } 20 \mathrm{~K} \\ & \text { RP124-320 } \end{aligned}$ | WA2G032S-203MA | A-B | 4610-10-7203 | 1 |
| R42 R43 R44 |  | RES, C, $1 / 4 \mathrm{~W}, 10 \%, 2.2 \mathrm{M}$ RC 104-522AB | CB2251 | A-B | 4705-16-2204 | 3 |
| R51 R52 |  | $\text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 3.3 \mathrm{~K}$ $\text { RC } 103-233$ | CF1/4-3.3k | ASE | 4700-15-3301 | 2 |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFER | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C01 103 | $\begin{aligned} & \text { CAP,F.T., 47OPF } \\ & \text { CF101-147 } \end{aligned}$ | FASC-4712 | A-B | 1510-30-0471 | 2 |
| co2 C15 | $\begin{aligned} & \text { CAP,F.T., } 6.8 P F \\ & \text { CF102-R68 } \end{aligned}$ | FA5C-6892 | A-B | 1510-30-1689 | 2 |
| ```C04 c05 C24 C26 c27 C29 c30``` | CAP, TANT, . 47MF, 50V CE113-447 | 935 | TRW | 1510-21-9470 | 7 |
| CO6 | CAP, MON, 1MF, 50V, $20 \%$ | 3420-050-E105M | AER | 1510-11-3105 | 1 |
| $\begin{array}{lllll} \text { c07 cos co9 C10 c14 } \\ \text { C16 } & \text { c22 } & \text { c3 } \end{array}$ | CAP, FT, CER, 100PF, $20 \%$ CF104-110 | 4420-100PF | AER | 1510-30-3101 | 8 |
| C11 C12 C20 | $\begin{aligned} & \text { CAP, Q-C, } 10 \mathrm{PF}, 10 \% \\ & \text { CG101-310 } \end{aligned}$ | QC-10PF | Q-C | 1510-40-0100 | 3 |
| C13 C21 | $\text { CAP, CER, 12OPF, } 1 \mathrm{KV}$ CD102-112 | 60U121M | MDC | 1510-10-1121 | 2 |
| C17 | $\begin{aligned} & \text { CAP, Q. C.,. } 47 P F \\ & \text { CG101-147 } \end{aligned}$ | QC-. 47PF | Q-C | 1510-40-0478 | 1 |
| C18 | $\begin{aligned} & \text { CAP, CHIP, 1PF, } 100 \mathrm{~V} \\ & \text { CC101-R10 } \end{aligned}$ | 3BN100S1ROC (S) | VAR | 1510-00-0010 | 1 |
| C19 | CAP, Q. C. , 3PF CG101-230 | QC-3PF | Q-C | 1510-40-0030 | 1 |
| C23 | $\begin{aligned} & \text { CAP, Q.C., 1PF } \\ & \text { CG101-210 } \end{aligned}$ | QC-1PF | Q-C | 1510-40-0010 | 1 |
| C25 C28 C31 | CAP, CER,F.T. 1000PF CF112-210 | 54-794-010-102P | SPEC | 1510-30-8102 | 3 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | C. M109 | $\begin{aligned} & \text { ASSEMBLY } \\ & 1114-00 . \end{aligned}$ <br> PAgE: |  |  | $\begin{array}{r} \mathrm{REV} \\ \mathrm{E} \end{array}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C32 | $\begin{aligned} & \text { CAP, Q-C, } 2 . \text { OPF, } 10 \% \\ & \text { CG101-220 } \end{aligned}$ | QC-2. OPF | Q-C | 1510-40-0020 | 1 |
| CR01 CR02 CR03 CR04 | DIODE DCOOO-008 | B8205 | APX | 4803-02-0004 | 4 |
| CR05 CR09 | DIODE DPOOO-040 | MA47980 | M-A | 4805-02-0001 | 2 |
| CRO6 CR10 | DIODE DG100-821 | 1N82AG | G-I | 4807-01-0082 | 2 |
| CR07 CR0日 CR11 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 3 |
| IC1 IC2 IC3 | IC, IC000-004 | N5741T | SIG | 7000-57-4101 | 3 |
| J1 | CONN JF000-005 | 37JR116-1 | S-C | 2110-03-0002 | 1 |
| L01 Li7 Li8 | TORRID, 10 TURN | LA009-010-1 | HYT | 1810-05-0004 | 3 |
| L02 L03 | FERRITE CHOKE LA009-010 | T1255-2 | HYT | 1810-05-0002 | 2 |
| $\begin{aligned} & \text { L04 L07 L09 L11 L12 } \\ & \text { L13 L15 L19 } \end{aligned}$ | RF CHOKE | CHOKE | W-I | 1819-99-9999 | 8 |
| L05 L08 L10 L14 | $\begin{aligned} & \text { CHOKE - 22MH } 10 \% \\ & \text { LAOO5-RO2 } \end{aligned}$ | O8NR22K | ASE | 1810-03-0228 | 4 |
| LO6 | $\begin{aligned} & \text { CHOKE, - 22MH, } 10 \% \\ & \text { LAOOB-RO2 } \end{aligned}$ | 506-000022V1 | SYS | 1810-04-0228 | 1 |
| L16 | TORRID, 4 TURN | LA009-004-1 | HYT | 1810-05-0003 | 1 |
| Q1 | TRANS QA054-610 | 2N5461 | MOT | 4901-05-4610 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | SC, M109 | ASSEMBLY $1114-00$ <br> PAGE: |  |  |  |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q2 | TRANS QBOOO-013 | A430 | APX | 4902-00-4300 | 1 |
| Q3 Q6 | TRANS QAO50-530 | 2N5053 | APX | 4901-05-0530 | 2 |
| Q4 | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 1 |
| Q5 | TRANS QA051-090 | 2N5109 | Sss | 4901-05-1090 | 1 |
| R01 R04 R16 R38 | $\text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 2.2 \mathrm{~K}$ RC 103-222 | CF1/4-2. 2 K | ASE | 4700-15-2201 | 4 |
| R03 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{M} \\ & \text { RC } 103-610 \end{aligned}$ | CB1065 | A-B | 4700-15-1005 | 1 |
| $\begin{array}{llll} \text { R02 } & \text { 111 } & \text { R17 } & \text { R22 } \\ \text { R30 } & \text { R37 } & \text { R40 } \end{array}$ | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K} \\ & \text { RC } 103-310 \end{aligned}$ | CF1/4-10K | ASE | 4700-15-1002 | 8 |
| R05 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 680$ RC 103-168 | CF1/4-680 | ASE | 4700-15-6800 | 1 |
| RO6 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 8.2 K$ RC 103-282 | CF $1 / 4-8.2 \mathrm{~K}$ | ASE | 4700-15-8201 | 1 |
| R07 R08 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{~K} \\ & \text { RC } 103-210 \end{aligned}$ | CF1/4-1K | ASE | 4700-15-1001 | 2 |
| R09 R12 R31 R33 | $\text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 4.7 \mathrm{~K}$ RC 103-247 | CF1/4-4.7K | ASE | 4700-15-4701 | 4 |
| R10 R32 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 470 \\ & \text { RC } 103-147 \end{aligned}$ | CF 1/4-470 | ASE | 4700-15-4700 | 2 |
| R13 R34 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 560$ RC 103-156 | CF1/4-560 | ASE | 4700-15-5600 | 2 |
| WAVETEK PARTS LIST | Sc, M109 | ASSEMBL $1114-00$ <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{E} \end{array}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK ND. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R14 R35 | POT, 20K, RP 129-320 | 360S203B | CTS | 4610-00-1203 | 2 |
| R15 | RES, C, 1/4W, 5\%, 470K RC 103-447 | CF1/4-470K | ASE | 4700-15-4703 | 1 |
| R18 | RES, $C, 1 / 4 W, 5 \%, 270$ RC 103-127 | CF1/4-270 | ASE | 4700-15-2700 | 1 |
| R19 R41 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 47$ RC 103-047 | CF 1/4-47 | ASE | 4700-15-4709 | 2 |
| R20 R26 | RES, C, 1/4W, 5\%, 3. 3K RC103-233 | CF1/4-3.3K | ASE | 4700-15-3301 | 2 |
| R21 R24 | $\begin{aligned} & \text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 15 \mathrm{~K} \\ & \text { RC } 103-315 \end{aligned}$ | CF 1/4-15K | ASE | 4700-15-1502 | 2 |
| R23 | RES, C, 1/4W, 5\%, 91K RC 103-391 | CF1/4-91K | ASE | 4700-15-9102 | 1 |
| R25 R39 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{~K} \\ & \text { RC } 103-347 \end{aligned}$ | CF1/4-47K | ASE | 4700-15-4702 | 2 |
| R28 | RES, C, $1 / 2 W, 5 \%, 150$ RC 105-115 | CF1/2-150 | ASE | 4700-25-1500 | 1 |
| R29 | RES, C, 1/4W, 5\%, 3. 9K RC 103-239 | CF1/43.9K | ASE | 4700-15-3901 | 1 |
| R36 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 100 \mathrm{~K}$ RC 103-410 | CF1/4-100K | ASE | 4700-15-1003 | 1 |
| WAVETEK PARTS LIST | SC, M109 | ASSEMBLY <br> 1114-00 <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{E} \end{array}$ |




| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK No. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C201 C207 | CAP, TANT, . 47MF, 50 V CE113-447 | 935 | TRW | 1510-21-9470 | 2 |
| C202 c204 c206 | CAP, FT, 500PF, 20\%250V CF104-150 | 4420-500PF | AER | 1510-30-3501 | 3 |
| C203 | CAP, ELECT, 1MF, 25 V CE120-001 | 162D105×9025BC2 | SPR | 1510-21-7010 | 1 |
| C205 | $\begin{aligned} & \text { CAP, Q-C, } 2 . \text { OPF, } 10 \% \\ & \text { CG101-220 } \end{aligned}$ | QC-2. OPF | Q-C | 1510-40-0020 | 1 |
| CR201 | DIODE DBOOO-001 | HW6. 88 | MSP | 4801-02-0001 | 1 |
| CR202 | DIODE DCOOO-005 | BBI41A | ITT | 4889-00-0001 | 1 |
| L201 L203 | RF CHOKE | CHOKE | W-I | 1819-99-9999 | 2 |
| L204 L206 | FERRITE CHOKE LA009-010 | T1255-2 | HYT | 1810-05-0002 | 2 |
| Q201 Q202 | TRANS QAOSO-530 | 2N5053 | APX | 4901-05-0530 | 2 |
| 0203 | TRANS GBOOO-009 | MPS3702 | MOT | 4902-03-7020 | 1 |
| Q204 | TRANS GBOOO-013 | A430 | APX | 4902-00-4300 | 1 |
| R201 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 100$ RC103-110 | CF1/4-100 | ASE | 4700-15-1000 | 1 |
| R202 | $\text { RES, } C, 1 / 4 W, 5 \%, 330$ RC103-133 | CF1/4-330 | ASE | 4700-15-3300 | 1 |
| WAVETEK PARTS LIST | MP , A529-012 | $\begin{aligned} & \text { ASSEMBLY } \\ & 1219-00 \end{aligned}$ <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{D} \end{array}$ |




| REFERENCE DESIGNATOR | PART DESCRIPTION | ORIG-MFGR-PART--NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CROG CRO7 CROB CRO9 CRIO CR11 | DIODE DPOOO-060 | MA47047 | M-A | 4805-02-0003 | 6 |
| CR16 CR17 | DIODE, VARACTOR DCOOO-010 | DKV65508 | AIN | 4803-02-0006 | 2 |
| CR18 CR19 CR24 CR25 | DIODE DPOOO-040 | MA47980 | M-A | 4805-02-000i | 4 |
| CR20 CR21 CR22 CR23 | DIODE DROOO-001 | 1N4004 | $\mathrm{F}-\mathrm{C}$ | 4806-01-4004 | 4 |
| J1 J2 | CONiN .JF000-005 | 37JR116-1 | S-c | 2110-03-0002 | 2 |
| L01 L02 L05 L06 Lib | $\begin{aligned} & \text { CHOKE 2EMH } 10 \% \\ & \text { LAOO5-RO2 } \end{aligned}$ | 08NR22K | ASE | 1810-03-0228 | 5 |
| L03 L04 L07 L08 Lio | RF CHDKE | CHOKE | W-I | 1819-99-9999 | 10 |
| L09 | $\begin{aligned} & \text { CHOKE 1ONH } 10 \% \\ & \text { LAOOS-RO1 } \end{aligned}$ | OBNR 10 OK | ASE | 1810-03-0019 | 1 |
| 117 | TORRID, 10 TURN | LA007-010-1 | hyt | 1810-05-0004 | 1 |
| Q01 | TFANS QBOOO-034 | BFR94 | APX | 4902-00-0940 | 1 |
| Q02 | TRAINS QBOOO-013 | A430 | APX | 4902-00-4300 | 1 |
| Q03 004 006 008 012 | TRANS QBOOO-009 | MF53702 | MOT | 4902-03-7020 | 5 |
| 005 | TRANS QBOOO-033 | MRF905 | MOT | 4902-00-9050 | 1 |
| Q07 Q13 | TRANS QAO54-610 | 2N5461 | MOT | 4901-05-4610 | 2 |
| WAVETEK PARTS LIST | $\begin{aligned} & \text { TITLE } \\ & \text { SWP OSC,M1:0 } \end{aligned}$ | $\begin{aligned} & \text { ASSEMBLY } \\ & \text { i114-OC } \end{aligned}$ |  |  | $\mathrm{REV}_{\mathrm{F}}$ |
|  |  | PAGE: 2 |  |  |  |





| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFGR- | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L7 |  | $\begin{aligned} & \text { CHOKE, } 22 M H, 10 \% \\ & \text { LA005-022 } \end{aligned}$ | 08N220 | ASE | 1810-03-0220 | 1 |
| Q1 Q2 Q3 Q4 |  | TRANS MCRWV | NE02135 | NEC | 4902-02-1350 | 4 |
| Q5 06 |  | TRANS PWR | MSC80264 | MSC | 4902-80-2640 | 2 |
| R01 |  | RES, C, 1/8W, 5\%, 120 | BB 1215 | A-B | 4705-05-1200 | 1 |
| R02 R08 R10 |  | RES, C, 1/4W, 5\%, 470 RC 103-147 | CF 1/4-470 | ASE | 4700-15-4700 | 3 |
| R03 R07 R09 R11 R12 |  | RES, C, 1/8W, 5\%, 330 | B83315 | A-B | 4705-05-3300 | 5 |
| R04 R13 |  | RES, C, 1/8W, 5\%, 75 | BB7505 | A-B | 4705-05-7509 | 2 |
| R05 |  | RES, C, $1 / 8 \mathrm{~W}, 5 \%, 100$ | BB1015 | A-B | 4705-05-1000 | 1 |
| R06 |  | RES, C, 1/8W, 5\%, 180 | BB1815 | A-B | 4705-05-1800 | 1 |
| R14 |  | RES, C3, 1/8W, $1 \% .49 .9$ RF220-499 | C3-49.9 | CGW | 4706-03-4999 | 1 |
| R15 |  | RES, C, 1/8W, 5\%, 47 RC101-047 | CF1/8-47 | ASE | 4700-05-4709 | 1 |
| NONE |  | BIAS CKT ASSY | MA111-53 | W-I | 1218-00-1100 | 1 |
| NONE |  | I/O COUPLING NETWORK | MA111-52 | W-I | 1218-00-1110 | 1 |
| NONE |  | I/O COUPLING NETWORK | MA111-S1 | W-I | 1218-00-1111 | 1 |
| WAVETEK PARTS LIST | TITLE QUTPUT MA111 | AMPLIFIER |  |  |  | $\begin{array}{r} \mathrm{REV} \\ \mathrm{I} \end{array}$ |






| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK No. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COI | CAP, CER, F.T. 1000PF CF112-210 | 54-794-010-102P | SPEC | 1510-30-8102 | 1 |
| $\mathrm{CO2}$ | $\begin{aligned} & \text { CAP, CER, } 1 \text { OPF, } 1 \mathrm{KV} \\ & \text { CD101-010 } \end{aligned}$ | 10TCC-Q10 | SPR | 1510-10-0100 | 1 |
|  | CAP,F.T., 6. BPF CF102-R68 | FA5C-6892 | $A-B$ | 1510-30-1689 | 11 |
| C04 C14C15 | $\begin{aligned} & \text { CAP,F.T., 470PF } \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | $A-B$ | 1510-30-0471 | 3 |
| cos | CAP, MYLAR, . O22MF200V CP101-322 | WMF2S22 | $C-D$ | 1510-60-0223 | 1 |
| C13 C16 | CAP, TANT, 10MF, 25 V CE120-010 | 162D106×0025DD2 | SPR | 1510-21-7100 | 2 |
| CRO1 CRO2 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 2 |
| ICO1 ICO2 ICO4 | DUAL OP AMP, RAYTHEON IC000-027 | RC4558DN | RAY | 7000-45-5801 | 3 |
| 1 CO 3 | IC, IC000-030 | LM318N | NAT | 7000-03-1800 | 1 |
| L01 L02 | FERRITE CHOKE LA009-010 | T1255-2 | HYt | 1810-05-0002 | 2 |
| RO1 | RES, MF, $1 / 8 \mathrm{~W}, 1 \%, 47.5 \mathrm{~K}$ RF213-475 | MF55K-47. 5 K | ASE | 4701-03-4752 | 1 |
| R02 | $\begin{aligned} & \text { RES, MF, } 1 / 8 \mathrm{~W}, 1 \%, 46.4 \mathrm{~K} \\ & \text { RF213-464 } \end{aligned}$ | MF55K-46.4K | ASE | 4701-03-4642 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | $\begin{aligned} & \text { TITLE } \\ & \text { MODULATOR, M121 } \end{aligned}$ | ASSEMBLY $1114-00$ <br> PAGE: |  |  | $\begin{array}{r} \mathrm{REV} \\ \mathrm{~F} \end{array}$ |





| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NQ. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ICO1 1C02 1C03 1C04 |  | DUAL OP AMP, RAYTHEON IC000-027 | RC4558DN | RAY | 7000-45-5801 | 4 |
| Q01 Q02 Q04 |  | TRANS QA054-580 | 2N5458 | MOT | 4901-05-4580 | 3 |
| Q03 Q05 |  | TRANS QA054-610 | 2N5461 | MOT | 4901-05-4610 | 2 |
| $\begin{aligned} & \text { Q06 Q08 Q10 Q11 Q12 } \\ & \text { Q13 } \end{aligned}$ |  | TRANS QBOOO-009 | MPS3702 | MOT | 4902-03-7020 | 6 |
| Q07 Q09 |  | TRANS QAO3B-541 | 2N3854A | G-E | 4901-03-8541 | 2 |
| Q14 Q15 Q16 Q17 |  | TRANS QA039-040 | 2N3904 | T-I | 4901-03-9040 | 4 |
| R01 R02 R03 |  | RES, SET, 3-178K, 1/8W QTY: 3: 4701-03-1783 | R×000-002 | W-I | 4789-00-0001 | 1 |
| R04 R05 R06 R07 |  | RES, SET, 464K-MTCH. $1 \%$ QTY: 4: 4701-03-4643 | 4789-00-0008 | $\mathrm{W}-\mathrm{I}$ | 4789-00-0008 | 1 |
| R08 R10 R21 R24 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{M}$ RC 103-610 | CB1065 | A-B | 4700-15-100: | 4 |
| R11 R19 R9 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{M}$ RC 103-647 | CB4765 | A-B | 4700-15-4705 | 3 |
| R12 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 200 \mathrm{~K}$ RC 103-420 | CF $1 / 4-200 \mathrm{~K}$ | ASE | 4700-15-2003 | 1 |
| R13 R38 |  | RES, SET, 2-178K, 1/8W QTY: 2: 4701-03-1783 | R×000-005 | W-I | 4789-00-0002 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | TITLE <br> BAND | SELECT, M131 | ASSEMBLY $1114-00$ <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{C} \end{array}$ |



| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R30 |  | RES, MF, $1 / 8 \mathrm{~W}, 1 \%, 21$. 5 K RF213-215 | MF55K-21.5K | ASE | 4701-03-2152 | 1 |
| R31 |  | RES, MF, $1 / 8 \mathrm{~W} .1 \%, 9.09 \mathrm{~K}$ RF212-909 | MF55K-9.09K | ASE | 4701-03-9091 | 1 |
| R33 |  | RES, MF, $1 / 8 \mathrm{~W}, 1 \%, 16$. 5 K RF213-165 | MF55K-16.5K | ASE | 4701-03-1652 | 1 |
| $R 35$ |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 360 \mathrm{~K}$ RC 103-436 | CF1/4-360K | ASE | 4700-15-3603 | 1 |
| R37 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 620K RC 103-462 | CB6245 | A-B | 4700-15-6203 | 1 |
| R39 |  | RES, C, 1/4W, 5\%, 180K RC103-418 | CF1/4-180K | ASE | 4700-15-1803 | 1 |
| R41 R74 |  | $\text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 270 \mathrm{~K}$ RC103-427 | CF1/4-270K | ASE | 4700-15-2703 | 2 |
| R43 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 390 \mathrm{~K}$ RC 103-439 | CF1/4-390K | ASE | 4700-15-3903 | 1 |
| R46 R58 R68 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 100 \mathrm{~K}$ RC103-410 | CF1/4-100K | ASE | 4700-15-1003 | 3 |
| R47 R50 R61 R64 R70 R71 R79 R80 R81 R83 R96 R97 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC103-310 | CFi/4-10K | ASE | 4700-15-1002 | 12 |
| R48 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 3.3 \mathrm{~K}$ RC 103-233 | CF1/4-3.3k | ASE | 4700-15-3301 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | ```TITLE BAND SELECT, M131``` |  | ASSEMBLY <br> 1114-00 <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{C} \end{array}$ |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK No. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| co1 co2 co3 c04 cos <br> c06 c09 C10 C11 C12 | CAP, F.T., 6. BPF CF102-R68 | FA5C-6892 | A-B | 1510-30-1689 | 14 |
| C07 608 | $\begin{aligned} & \text { CAP, F.T., } 47 \text { OPF } \\ & \text { CF101-147 } \end{aligned}$ | FASC-4712 | A-B | 1510-30-0471 | 2 |
| C17 C18 | CAP, TANT, 10MF, 25 V CE120-010 | 162D106×0025DD2 | SPR | 1510-21-7100 | 2 |
| CRO1 CRO2 CRO3 CRO4 CRO5 CRO6 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 6 |
| ```Q01 Q03 Q05 Q08 Q10 Q11 Q12 Q13``` | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 8 |
| Q02 Q04 Q06 007 009 | TRANS QBOOO-009 | MPS3702 | MOT | 4902-03-7020 | 5 |
| R01 R05 R09 | RES, C, $1 / 4 \mathrm{~W}, 5 \%$, 82 K RC 103-382 | CF1/4-82K | ASE | 4700-15-8202 | 3 |
| R02 R04 R06 R08 R10 $R 12$ | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 15 \mathrm{~K}$ RC 103-315 | CF1/4-15K | ASE | 4700-15-1502 | 6 |
| R03 R07 R11 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 51 \mathrm{~K}$ RC103-351 | CF1/4-51k | ASE | 4700-15-5102 | 3 |
| R13 R17 | $\text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 100 \mathrm{~K}$ RC103-410 | CF1/4-100K | ASE | 4700-15-1003 | 2 |
| R14 R27 | $\text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 22 \mathrm{~K}$ RC 103-322 | CF1/422K | ASE | 4700-15-2202 | 2 |
| WAVETEK PARTS LIST | FACE, M132 | ASSEMBLY <br> 1114-00 <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{A} \end{array}$ |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFER | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | $\begin{aligned} & \text { CAP, F. T. , 47OPF } \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | A-B | 1510-30-0471 | 1 |
| C 2 | CAP, FT, 500PF, $20 \% 250 \mathrm{~V}$ CF104-150 | 4420-500PF | AER | 1510-30-3501 | 1 |
| C3 | $\text { CAP, CER, . O1MF, } 100 \mathrm{~V}$ CD103-310 | 68U103M | MDC | 1510-10-2103 | 1 |
| C4 | $\begin{aligned} & \text { CAP, CER , . O5MF, } 100 \mathrm{~V} \\ & \text { CD103-350 } \end{aligned}$ | TG-S50 | SPR | 1510-10-2503 | 1 |
| C5 | $\begin{aligned} & \text { CAP,F.T., } 6.8 P F \\ & \text { CF102-R68 } \end{aligned}$ | FA5C-6892 | A-B | 1510-30-1689 | 1 |
| CR1 | DIODE DG100-821 | 1 N82AG | G-I | 4807-01-0082 | 1 |
| J1 J2 J3 | CONN JFOOO-005 | 37JR116-1 | S-C | 2110-03-0002 | 3 |
| LO1 | TORRID, 4 TURN | LA009-004-1 | HYT | 1810-05-0003 | 1 |
| Q1 | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 1 |
| R01 | ```RES, C, 1/4W, 5%,47 RC103-047``` | CF1/4-47 | ASE | 4700-15-4709 | 1 |
| R02 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 51 \\ & \text { RC } 103-051 \end{aligned}$ | CFI/451 | ASE | 4700-15-5109 | 1 |
| R03 R05 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 470 \\ & \text { RC 103-147 } \end{aligned}$ | CF1/4-470 | ASE | 4700-15-4700 | 2 |
| R04 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 150 \\ & \text { RC 103-115 } \end{aligned}$ | CF1/4-150 | ASE | 4700-15-1500 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | $\text { TITLE }_{\text {EXT }}^{\text {MKR, M }}$ | ASSEMBLY NO. $1114-00-0124$ <br> PAGE: 1 |  |  | REV $\mathbf{B}$ |


| REFERENCE DESIGNATORS |  | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK ND. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RO6 |  | RES, C, 1/4W, 5\%, 180K RC 103-418 | CF1/4-180K | ASE | 4700-15-1803 | 1 |
| R07 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 470 \mathrm{~K}$ RC 103-447 | CF1/4-470K | ASE | 4700-15-4703 | 1 |
| R08 R10 |  | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC 103-310 | CF1/4-10K | ASE | 4700-15-1002 | 2 |
| R09 |  | $\begin{aligned} & \text { POT, } 20 \mathrm{~K} \\ & \text { RP 124-320 } \end{aligned}$ | WA2G0325-203MA | A-B | 4610-10-7203 | 1 |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C01 | CAP, VALUE DETERMINED IN CALIBRATION | CAP, TRIM | W-I | 1519-99-9999 | 1 |
| CO 2 | $\begin{aligned} & \text { CAP, CER, 33PF, } 1 \mathrm{KV} \\ & \text { CD104-033 } \end{aligned}$ | 10TU-033 | SPR | 1510-10-3330 | 1 |
| Co3 C14 | $\begin{aligned} & \text { CAP, CER, . O1MF, } 100 \mathrm{~V} \\ & \text { CD103-310 } \end{aligned}$ | 68U103M | MDC | 1510-10-2103 | 2 |
| C04 | CAP, CER, . 025MF,50V CD103-325 | TG-S25 | SPR | 1510-10-2253 | 1 |
| cos | CAP, CER, 68PF, 1KV CD104-068 | 6802 J 680 J | MDC | 1510-10-3680 | 1 |
| cob | CAP, CER, 100PF, 1 KV CD104-110 | 10TCU-T10 | SPR | 1510-10-3101 | 1 |
| 607 | CAP, VAR, 3.5-13PF250V CV101-013 | 7S-TRIKO-02-3.5-13PF | STR | 1510-70-0130 | 1 |
| C08 | $\begin{aligned} & \text { CAP, CER, 15PF, } 1 \mathrm{KV} \\ & \text { CD101-015 } \end{aligned}$ | 10TCC-Q15 | SPR | 1510-10-0150 | 1 |
| $\operatorname{cog}$ | CAP, CER, 4TPF, 1 KV CD104-047 | 60 V 2 J 470 J | MDC | 1510-10-3470 | 1 |
| C10 C13 | $\begin{aligned} & \text { CAP, CER, } 001 \mathrm{MFD}, 1 \mathrm{KV} \\ & \text { CD102-210 } \end{aligned}$ | 5GAD10 | SPR | 1510-10-1102 | 2 |
| C11 | CAP, TANT, . 47MF, 50 V CE113-447 | 935 | TRW | 1510-21-9470 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | $\text { TITLE } \underset{\text { MiKR, M6H-1 }}{ }$ | ASSEMBLY NO. <br> 1114-00-0050 <br> PAGE: 1 |  |  | $\underset{\mathrm{F}}{\mathrm{REV}}$ |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK ND. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q7 | TRANS QAO50-880 | 2N5088 | MOT | 4901-05-0880 | 1 |
| R01 R16 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{~K}$ RC103-210 | CF $1 / 4-1 \mathrm{~K}$ | ASE | 4700-15-1001 | 2 |
| R02 R05 R12 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 3.9 \mathrm{~K}$ RC 103-239 | CF1/43.9K | ASE | 4700-15-3901 | 3 |
| RO 3 RO 4 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 2.2 \mathrm{~K}$ RC 103-222 | CF1/4-2. 2 K | ASE | 4700-15-2201 | 2 |
| ROG | RES, C, 1/4W, 5\%, 27K RC 103-327 | CF1/4-27k | ASE | 4700-15-2702 | i |
| R07 R09 R13 | $\begin{aligned} & \text { RES, } C, 1 / 4 W, 5 \%, 470 \\ & \text { RC } 103-147 \end{aligned}$ | CF $1 / 4-470$ | ASE | 4700-15-4700 | 3 |
| R08 R20 | RES, C, 1/4W, $5 \%$, 1OK RC103-310 | CF1/4-10K | ASE | 4700-15-1002 | 2 |
| R10 R24 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 100 \\ & \text { RC103-110 } \end{aligned}$ | CF1/4-100 | ASE | 4700-15-1000 | 2 |
| R11 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 75 \\ & \text { RC103-075 } \end{aligned}$ | CR1/4-75 | ASE | 4700-15-7509 | 1 |
| R14 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 33 \mathrm{~K}$ RC 103-333 | CF1/4-33K | ASE | 4700-15-3302 | 1 |
| R15 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{M}$ RC103-510 | CF1/4-1M | ASE | 4700-15-1004 | 1 |
| R17 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 8$. 2 K RC103-282 | CF1/4-8. 2 K | ASE | 4700-15-8201 | i |
| WAVETEK PARTS LIST | R, M6H-1 | $\begin{gathered} \text { ASSEMBL } \\ 1114-00 \end{gathered}$ <br> PAGE: |  |  | $\underset{\mathrm{F}}{\mathrm{REV}}$ |




| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK No. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CR1 | DIODE DG100-821 | 1 N82AG | G-I | 4807-01-0082 | 1 |
| J1 J2 | CONN JFOOO-005 | 37JR116-1 | S-C | 2110-03-0002 | 2 |
| L1 L3 | RF CHOME | CHOKE | W-I | 1819-99-9999 | 2 |
| L02 | TORRID, 10 TURN | LA009-010-1 | HYT | 1810-05-0004 | 1 |
| L04 | TORRID, 4 TURN | LA009-004-1 | HYT | 1810-05-0003 | i |
| Q1 | TRANS QAO38-541 | 2N3854A | G-E | 4901-03-8541 | 1 |
| Q2 | TRANS QBOOO-013 | A430 | $A P X$ | 4502-00-4300 | 1 |
| Q3 | TRANS QA054-580 | 2N5458 | MOT | 4901-05-4580 | i |
| Q4 | TRANS QA050-880 | 2N5088 | MOT | 4901-05-0880 | i |
| RO1 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{~K} \\ & \text { RC } 103-347 \end{aligned}$ | CF1/4-47K | ASE | 4700-15-4702 | 1 |
| R02 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 56$ RC103-056 | CF1/4-56 | ASE | 4700-15-5609 | 1 |
| R03 | RES, C, 1/4W, 5\%, 1. 5K RC103-215 | CF1/4-1.5K | ASE | 4700-15-1501 | 1 |
| RO4 R17 | $\begin{aligned} & \text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 100 \\ & \text { RC } 103-110 \end{aligned}$ | CF $1 / 4$-100 |  | 4700-15-1000 | 2 |
| R05 | RES, C, 1/4W, 5\%, 75 RC 103-075 | CR1/4-75 | ASE | 4700-15-7509 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | $K \mathrm{R}, \mathrm{M} 6 \mathrm{H}-10$ | $\begin{aligned} & \text { ASSEMBLY } \\ & 1114-00 \end{aligned}$ <br> PAGE: |  |  | $\begin{gathered} \text { REV } \\ \mathrm{D} \end{gathered}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R06 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 3.9 \mathrm{~K} \\ & \text { RC } 103-239 \end{aligned}$ | CF1/43.9K | ASE | 4700-15-3901 | 1 |
| R07 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 470 \\ & \text { RC 103-147 } \end{aligned}$ | CF1/4-470 | ASE | 4700-15-4700 | 1 |
| R08 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 33 \mathrm{~K}$ RC 103-333 | CF1/4-33K | ASE | 4700-15-3302 | 1 |
| R09 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, \mathrm{im} \\ & \text { RC } 103-510 \end{aligned}$ | CFI/4-1M | ASE | 4700-15-1004 | 1 |
| Kio | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{k}$ RC 103-210 | CF1/4-1K | ASE | 4700-15-1001 | 1 |
| R11 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 8.2 \mathrm{~K}$ RC103-282 | CF1/4-8. 2 K | ASE | 4700-15-8201 | 1 |
| R12 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 15 \mathrm{~K} \\ & \text { RCi03-315 } \end{aligned}$ | CF1/4-15K | ASE | 4700-15-1502 | 1 |
| R13 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1.5 \mathrm{M}$ RC 103-515 | CF1/4-1.5M | ASE | 4700-15-1504 | 1 |
| R14 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K} \\ & \text { RC } 103-310 \end{aligned}$ | CF1/4-10K | ASE | 4700-15-1002 | 1 |
| R15 | $\begin{aligned} & \text { Pot, } 20 \mathrm{~K} \\ & \text { RP } 124-320 \end{aligned}$ | WA2G032S-203MA | A-B | 4610-10-7203 | 1 |
| R16 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 100 \mathrm{~K}$ RC103-410 | CF1/4-100K | ASE | 4700-15-1003 | 1 |
| X1 | CRYSTAL, XX000-321 | X32W-00.00000 | W-I | 2310-00-0321 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | $\begin{aligned} & \text { TITLE } \\ & \text { HAR MKR, MOH-10 } \end{aligned}$ | ASSEMBLY NO. $1114-00-0099$ <br> PAGE: 3 |  |  | $\begin{gathered} \text { REV } \\ \hline \end{gathered}$ |


| REFERENSE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COI | CAP, CER, 2OPF, 1KV CD101-020 | 60006200 J | MDC | 1510-10-0200 | 1 |
| C02 | $\text { CAP, CER, 120PF, } 1 \mathrm{KV}$ CD104-112 | 1OTCU-T12 | SPR | 1510-10-3121 | i |
| co3 C07 | $\begin{aligned} & \text { CAP, CER, } 47 P F, 1 K V \\ & \text { CD104-047 } \end{aligned}$ | $60 \cup 2 \mathrm{~J} 470 \mathrm{~J}$ | MDC | 1510-10-3470 | 2 |
| C04 | CAP, FT, 5000PF, $20 \% 250 \mathrm{~V}$ CF104-150 | 4420-500PF | AER | 1510-30-3501 | 1 |
| C05 | CAP, VAR, 3. 5-13PF250V CV101-013 | 7S-TRIKO-02-3. 5-13PF | STR | 1510-70-0130 | 1 |
| cob | CAP, CER, 15PF, 1KV CD101-015 | 10TCC-Q15 | SPR | 1510-10-0150 | 1 |
| $\cos \operatorname{cog}$ | $\begin{aligned} & \text { CAP, CER, } 001 \mathrm{MFD}, 1 \mathrm{KV} \\ & \text { CD102-210 } \end{aligned}$ | 5GAD10 | SPR | 1510-10-1102 | 2 |
| C10 | $\begin{aligned} & \text { CAP, CER,.01MF, 100V } \\ & \text { CD103-310 } \end{aligned}$ | 68U103M | MDC | 1510-10-2103 | 1 |
| C11 | CAP, F. T. , 6. BPF CF102-R68 | FA5C-6892 | $A-B$ | $1510-30-1689$ | 1 |
| C12 | $\begin{aligned} & \text { CAP,F.T., 470PF } \\ & \text { CF101-147 } \end{aligned}$ | FA5C-4712 | $A-B$ | 1510-30-0471 | 1 |
| C13 | CAP, TANT, $10 \mathrm{MF}, 25 \mathrm{~V}$ CE120-010 | 162D106×0025DD2 | SPR | 1510-21-7100 | i |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | KR, M6H-50 | $\begin{aligned} & \text { ASSEMBLYNO. } \\ & 1114-00-01 \end{aligned}$ <br> PAGE: 1 |  |  | $\underset{\mathrm{E}}{\mathrm{REV}}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIE-MFGR-PART-HO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CR 1 | DIODE DG100-821 | 1 Ng2AG | G-I | 4807-01-0082 | 1 |
| Ji J2 | CONV JF000-005 | 37JR116-1 | S-C | 21i0-03-0002 | 2 |
| Li L3 | RF CHOKE | CHOKE | W-I | 1819-99-9999 | 2 |
| L02 | TORRID, 10 TURN | LA009-010-1 | HYT | 1810-05-0004 | 1 |
| L04 | TORRID, 4 TURN | LA009-004-1 | HYT | 1810-05-0003 | 1 |
| Q01 | TRANS QA039-040 | 2N3904 | T-I | 4901-03-9040 | 1 |
| Q2 | TRANS QBOOO-013 | A430 | APX | 4902-00-4300 | 1 |
| Q3 | TRANS QAO54-580 | 2N5458 | MOT | 4901-05-4580 | 1 |
| Q4 | TRANS QA050-880 | 2N5088 | MOT | 4901-05-0880 | 1 |
| R01 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{~K}$ RC 103-347 | CF $1 / 4-47 \mathrm{~K}$ | ASE | 4700-15-4702 | 1 |
| R02 | RES, C, 1/4W, 5\%, 56 RC 103-056 | CF1/4-56 | ASE | 4700-15-5609 | 1 |
| R03 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1.5 K$ RC 103-215 | CF 1/4-1.5K | ASE | 4700-15-1501 | 1 |
| R04 R17 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 100 \\ & \text { RC103-110 } \end{aligned}$ | CF1/4-100 | ASE | 4700-15-1000 | 2 |
| R05 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 75 \\ & \text { RC } 103-075 \end{aligned}$ | CR1/4-75 | ASE | 4700-15-7509 | 1 |
| WAVETEK | HARLE MKR, M6H-50 | ASSEMBLY NO.$1114-00-0100$ |  |  | $\underset{E}{\text { REV }}$ |
|  |  | PAGE: 2 |  |  |  |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK No. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RO 6 | $\text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 3.9 \mathrm{~K}$ RC103-239 | CFi/43.9K | ASE | 4700-15-3901 | 1 |
| R07 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 470 \\ & \text { RC } 103-147 \end{aligned}$ | CF $1 / 4-470$ | ASE | 4700-15-4700 | 1 |
| ROE | $\begin{aligned} & \text { RES, } C, 1 / 4 \mathrm{~W}, 5 \%, 33 \mathrm{~K} \\ & \text { RC } 103-333 \end{aligned}$ | CF1/4-33K | ASE | 4700-15-3302 | 1 |
| R09 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{M} \\ & \text { RC } 103-510 \end{aligned}$ | CF1/4-1M | ASE | 4700-15-1004 | 1 |
| R10 | RES, C, 1/4W, 5\%, 1K RC103-210 | CFI/4-1K | ASE | 4700-15-1001 | 1 |
| R11 | $\begin{aligned} & \text { RES, } C, 1 / 4 W, 5 \%, 8.2 K \\ & \text { RC } 103-282 \end{aligned}$ | CF 1/4-8. 2 K | ASE | 4700-15-8201 | 1 |
| R12 | RES, C, 1/4W, 5\%, 15K RC 103-315 | CF1/4-15K | ASE | 4700-15-1502 | 1 |
| R13 | RES, C, 1/4W, 5\%, 1.5M RC 103-515 | CF1/4-1.5M | ASE | 4700-15-1504 | 1 |
| R14 | RES, $\mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K}$ RC103-310 | CF1/4-10K | ASE | 4700-15-1002 | 1 |
| R15 | $\begin{aligned} & \text { POT, } 20 \mathrm{~K} \\ & \text { RP } 124-320 \end{aligned}$ | WA290325-203MA | $A-B$ | 4610-10-7203 | 1 |
| R16 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 100 \mathrm{~K}$ RC103-410 | CF1/4-100K |  | 4700-15-1003 | 1 |
| X1 | CRYSTAL, XX000-331 | X $33 W-00.00000$ | W-I | 2310-00-0331 | 1 |
| $\begin{aligned} & \text { WAVETEK } \\ & \text { PARTS LIST } \end{aligned}$ | TITLE <br> HAR MKR, M6H-50 |  |  |  | $\underset{\mathrm{E}}{\mathrm{REV}}$ |



| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | $\begin{aligned} & \text { CHOKE, 2. } 2 \mathrm{MH}, 10 \% \\ & \text { LAOO5-R22 } \end{aligned}$ | O8N2R2K | ASE | 1810-03-0229 | 1 |
| Q1 Q2 | TRANS QAOS8-54i | 2N3854A | G-E | 4901-03-854i | 2 |
| R1 | $\begin{aligned} & \text { RES, } \mathrm{C}, 1 / 4 \mathrm{~W}, 5 \%, 47 \mathrm{~K} \\ & \text { RC 103-347 } \end{aligned}$ | CF $1 / 4-47 \mathrm{~K}$ | ASE | 4700-15-4702 | 1 |
| R2 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 56 \\ & \text { RC } 103-056 \end{aligned}$ | CF1/4-56 | ASE | 4700-15-5609 | 1 |
| R3 R4 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1.5 \mathrm{~K}$ RC 103-215 | CF1/4-1.5K | ASE | 4700-15-1501 | 2 |
| R5 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 180 \mathrm{~K}$ RC103-418 | CF1/4-180K | ASE | 4700-15-1803 | i |
| R6 | ```RES, C, 1/4W,5%,470K RC 103-447``` | CF1/4-470K | ASE | 4700-15-4703 | 1 |
| R7 R9 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 10 \mathrm{~K} \\ & \text { RC } 103-310 \end{aligned}$ | CF $1 / 4-10 \mathrm{C}$ | ASE | 4700-15-1002 | 2 |
| Rg | FOT, 20K <br> RP 124-320 | WA2G0325-203mA | $A-B$ | 4610-10-7203 | i |
| $x 1$ | CRYSTAL, XX000-331 | X33W-00.00000 | W-I | 2310-00-0331 | 1 |
| WAVETEK | RR, M6S-3 | $\begin{array}{r} \text { ASSEMBL } \\ 1114-00 \end{array}$ |  |  | $\underset{A}{\operatorname{REV}}$ |




| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C43 | CAP, VAR, 2.5/5PF | 5S-TRIKO-04-2.5/5 | STR | 1510-70-8509 | 1 |
| CRO1 CRO2 | DIODE DGOOO-007 | 5082-2800 | $\mathrm{H}-\mathrm{P}$ | 4809-02-0001 | 2 |
| CR03 | DIODE DGOOO-012 | 5082-0180 | $\mathrm{H}-\mathrm{P}$ | 4811-02-0001 | 1 |
| CR4 | DIODE DG100-821 | 1 N82AG | G-I | 4807-01-0082 | 1 |
| ICOI | IC, ICOOO-011 | 78m05uc | FCD | 7000-78-0500 | 1 |
| J01 J02 | CONN JFOOO-005 | 37JR116-1 | S-C | 2110-03-0002 | 2 |
| L01 L12 L13 L14 Li5 | $\begin{aligned} & \text { CHOKE . } 47 \mathrm{MH} \text { 10\% } \\ & \text { LAOO5-R04 } \end{aligned}$ | O8NR47K | ASE | 1810-03-0478 | 5 |
| L02 L03 L05 L06 L09 | $\begin{aligned} & \text { CHOKE . 22MH } 10 \% \\ & \text { LAOOS-RO2 } \end{aligned}$ | O8NR22K | ASE | 1810-03-0228 | 5 |
| L04 L07 | $\begin{aligned} & \text { CHOKE, } 1 \text { MH, } 10 \% \\ & \text { LAOOS-R10 } \end{aligned}$ | OBN1ROK | ASE | 1810-03-0010 | 2 |
| LOB | CHOKE, 3.3MH, 10\% LA005-R33 | O8N3R3K | ASE | 1810-03-0339 | 1 |
| L10 | RF CHOKE | CHOKE | W-I | 1819-99-9999 | 1 |
| L16 | CHOKE, . 82MH 10\% | O80R82K | ASE | 1810-03-0828 | 1 |
| Q1 Q3 Q4 Q5 Q6 | TRANS QAO50-530 | 2N5053 | AP X | 4901-05-0530 | 5 |
| 02 | TRANS QAOB8-541 | 2N3854A | G-E | 4901-03-8541 | 1 |
| R01 | RES, C, 1/4W, 5\%, 1. 8 K RC103-218 | CF1/4-1.8K | ASE | 4700-15-1801 | 1 |
| WAVETEK PARTS LIST | AR MKR, M106 | ASSEMBLY $1114-00$ <br> PAGE: |  |  |  |




| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-ND | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $C 101$ $C 103$ $C 104$ $C 106$ <br> C107 C108 C115   | CAP, ELECT, 1MF, 25 V CE120-001 | 162D105 9025 BC 2 | SPR | 1510-21-7010 | 7 |
| C102 | $\begin{aligned} & \text { CAP, CER, } 3.3 P F, 1 K V \\ & \text { CD101-R33 } \end{aligned}$ | 10TCC-V33 | SPR | 1510-10-0339 | 1 |
| C109 C112 C120 C123 | CAP, CER , . $01 \mathrm{MF}, 100 \mathrm{~V}$ CD103-310 | 68U103M | MDC | 1510-10-2103 | 4 |
| C110 | ```CAP, CER, 4. 7PF, 1KV CD101-R47``` | 10TCC-V47 | SPR | 1510-10-0479 | 1 |
| C111 C124 C125 | CAP, VAR, 3. 5-13PF250V CV101-013 | 7S-TRIKO-02-3. 5-13PF | STR | 1510-70-0130 | 3 |
| C113 C119 | CAP, CER , 36OPF, 1 KV CD102-136 | $60 \cup 361 \mathrm{M}$ | MDC | 1510-10-1361 | 2 |
| C114 C118 | CAP, CER, 470PF, 1 KV CD102-147 | $60 \cup 471 \mathrm{M}$ | MDC | 1510-10-1471 | 2 |
| C116 | $\begin{aligned} & \text { CAP, CER, . OO2MF, 1KV } \\ & \text { CD102-220 } \end{aligned}$ | 5GAD20 | SPR | 1510-10-1202 | 1 |
| C121 | $\begin{aligned} & \text { CAP, CER, 12OPF, } 1 \mathrm{KV} \\ & \text { CD102-112 } \end{aligned}$ | 60U121M | MDC | 1510-10-1121 | 1 |
| CR101 CR102 CR103 CR111 CR112 | DIODE DG109-140 | 1N4148 | FCD | 4807-01-0914 | 5 |
| CR106 | DIODE DG100-821 | 1N82AG | G-I | 4807-01-0082 | 1 |
| CR107 CR108 CR109 CR110 | DIODE DGOOO-007 | 5082-2800 | H-P | 4809-02-0001 | 4 |
| WAVETEK PARTS LIST |  | ASSEMBLY No. $1218-00-11$ <br> PAGE: 1 |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{D} \end{array}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IC101 | IC, IC000-017 | N82590A | SIG | 8000-82-9001 | 1 |
| IC102 | IC. IC000-016 | N8290A | SIG | 8000-82-9000 | 1 |
| IC103 | IC, IC000-012 | SN7404N | T-I | 8000-74-0400 | 1 |
| IC 104 | IC, IC000-005 | RC4558DN | RAY | 7000-14-5800 | 1 |
| L108 | $\begin{aligned} & \text { CHOKE . } 47 \mathrm{MH} \quad 10 \% \\ & \text { LAOO5-RO4 } \end{aligned}$ | O8NR47K | ASE | 1810-03-0478 | 1 |
| L301 L302 L303 | TORRID, 10 TURN | LA009-010-1 | HYT | 1810-05-0004 | 3 |
| Q103 Q104 Q108 Q109 | TRANS QAO50-530 | 2N5053 | APX | 4901-05-0530 | 4 |
| Q105 Q106 Q107 Q110 | TRANS QAO54-580 | 2N5458 | MOT | 4901-05-4580 | 4 |
| Q111 | TRANS QAO54-610 | 2N5461 | MOT | 4901-05-4610 | 1 |
| R101 R103 | RES, $1 / 8 \mathrm{~W}, 5,12 \mathrm{~K}-\mathrm{OHM}$ | CF1/8-12K | ASE | 4700-05-1202 | 2 |
| R105 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 390 \\ & \text { RC } 103-139 \end{aligned}$ | CF1/4-390 | ASE | 4700-15-3900 | 1 |
| R106 | RES, C, 1/8W, 5\%, 22 RC101-022 | CF1/8-22 | ASE | 4700-05-2209 | 1 |
| R107 | $\begin{aligned} & \text { RES, C, 1/8W, } 5 \%, 47 \\ & \text { RC101-047 } \end{aligned}$ | CF1/8-47 | ASE | 4700-05-4709 | 1 |
| R109 R112 R136 R140 | RES. C. $1 / 8 \mathrm{~W} 5 \% 470$ | CF1/8-470 | ASE | 4700-05-4700 | 4 |
| WAVETEK PARTS LIST |  | $\begin{aligned} & \text { ASSEMBLY } \\ & 1218-00 \end{aligned}$ <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{D} \end{array}$ |


| REFERENCE DESIGNATORS | PART DESCRIPTION | ORIG-MFGR-PART-NO | MFGR | WAVETEK NO. | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R110 R113 R115 R116 R118 R134 R135 R138 R139 | RES, C, 1/8W, $5 \%$, 1K RC101-210 | CF1/8-1K | ASE | 4700-05-1001 | 9 |
| R111 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 560$ RC 103-156 | CF1/4-560 | ASE | 4700-15-5600 | 1 |
| R114 R133 R137 | RES, C, 1/4W, 5\%, 180 RC103-118 | CF 1/4-180 | ASE | 4700-15-1800 | 3 |
| R117 R120 R130 R144 | POT, 20K, RP 144-320 | 91WR2OK | BEK | 4610-00-4203 | 4 |
| R119 R151 | RES, C, $1 / 4 \mathrm{~W}, 5 \%, 1 \mathrm{~K}$ RC103-210 | CF $1 / 4$ - 1 K | ASE | 4700-15-1001 | 2 |
| R121 R122 R124 R127 R145 | RES, C, 1/8W, 5\%, 4. 7K RC101-247 | CF1/8-4.7K | ASE | 4700-05-4701 | 5 |
| R123 R126 | RES, C, $1 / 8 \mathrm{~W}, 5 \%, 22 \mathrm{~K}$ RC101-322 | CF $1 / 8-22 \mathrm{~K}$ | ASE | 4700-05-2202 | 2 |
| R125 R128 R129 R143 | RES, C, $1 / 8 \mathrm{~W}, 5 \%, 10 \mathrm{M}$ RC101-610 | BB1065 | A-B | 4700-05-1005 | 4 |
| R131 R141 | $\begin{aligned} & \text { RES, C, } 1 / 4 \mathrm{~W}, 5 \%, 1.5 \mathrm{~K} \\ & \text { RC } 103-215 \end{aligned}$ | CF1/4-1.5K | ASE | 4700-15-1501 | 2 |
| R132 R146 | RES, C, $1 / 8 \mathrm{~W}, 5 \%$, 2 K RC101-220 | CF $1 / 8-2 \mathrm{~K}$ | ASE | 4700-05-2001 | 2 |
| R142 | RES, C, 1/4W, 5\%, 22K RC103-322 | CF $1 / 422 \mathrm{~K}$ | ASE | 4700-15-2202 | 1 |
| WAVETEK PARTS LIST |  | ASSEMBLY <br> 1218-00 <br> PAGE: |  |  | $\begin{array}{r} \text { REV } \\ \mathrm{D} \end{array}$ |



### 7.1 INTRODUCTION

This section contains all schematics for the instrument. A schematic index is given in Section 7.3.

### 7.2 SCHEMATIC NOTES

The following notes and abbreviations pertain to all sche-
matics. Additional notes pertaining to specific schematics are included on each schematic if required.

Unless otherwise noted, resistor values are given in ohms, capacitor values are given in pF , and inductor values are given in $\mu \mathrm{H}$.

## SYMBOL NOTES

Denotes DC voltage reading unless otherwise
specified.

| Denotes high-impedance crystal detector |
| :--- |
| reading in volts unless otherwise specified. |


| Denotes 50 ohm crystal detector reading in |
| :--- |
| volts unless otherwise specified. |

Arrow indicates clockwise rotation of wiper.


## ABBREVIATION CODE

| A | ampere | IF | intermediate frequency | $\Omega$ | ohm |
| :--- | :--- | :--- | :--- | :--- | :--- |
| AC | alternating current | J | jack | OC | opto-coupler |
| C | capacitor | K | relay | P | plug |
| ccw | counterclockwise | kHz | kilohertz | p | peak |
| CR | diode | $\mathrm{k} \Omega$ | kilohm | pp | peak-to-peak |
| CW | continuous wave | kV | kilovolt | pF | picofarad |
| cw | clockwise | kW | kilowatt | Q | transistor |
| dB | decibel | L | inductor | R | resistor |
| dBc | dB referred to carrier | M | meter | RF | radio frequency |
| dBm | dB referred to 1 mW | MHz | megahertz | RMS | root-mean-square |
| dBmV | dB referred to 1 mV | $\mathrm{M} \Omega$ | megohm | $\mathrm{R} . \mathrm{P}$. | rear panel |
| DC | direct current | mA | milliampere | S | switch |
| DS | indicating device, lamp | mH | millihenry | T | transformer |
| F | farad | mV | millivolt | $\mathrm{T} . \mathrm{P}$. | test point |
| $\mathrm{F} . \mathrm{P}$. | front panel | mW | milliwatt | V | volt |
| H | henry | $\mu \mathrm{F}$ | microfarad | VA | voltampere |
| Hz | hertz | $\mu \mathrm{A}$ | microampere | W | watt |
| IC | integrated circuit | $\mu \mathrm{H}$ | microhenry | X | crystal |

### 7.3 SCHEMATIC INDEX

The schematics appear in the following order.

| ASSEMBLY | NAME |
| :--- | :--- |
| 2002A | Wiring Diagram |
| 2002A | Marker System Diagram |
| DPS2A | Power Supply |
| M101B | Sweep Rate |
| M102A | Sweep Drive |
| M103A | Sweep Drive |
| M104A | Leveler |
| M105 | Marker Adder |
| M109 | Sweep Oscillator 1 |
| M110 | Sweep Oscillator 2A, 2B, 3 |
| MA111 | Output Amplifier |
| M121 | Modulator |
| M131 | Band Select |
| M132 | Interface |
| M6C | External Marker |
| M6H-1 | Harmonic Marker (1 MHz) |
| M6H-5-50 | Harmonic Marker (5-50 MHz) |
| M6S | Single Frequency Marker |
| M106 | Deluxe Harmonic Marker |

Printed circuit board layouts, where applicable, are shown opposite their corresponding schematics.





## M 101B




## M102A




## M103A




M104A



## M 105







M121




M132





REV D


REV $\qquad$


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## M106




Pg 5-13 $\quad 1500 \mathrm{MHz}$ crossover adj. is R63, not R64.
M131 R17 and R45 are now CTS, 363T105B, Wavetek P/N 4610-00-3105.
M104A R10 and R29 are now 100 kohm, Wavetek P/N 4700-15-1003.
R30 and R41 (see schematic details) are 1 Mohm potentiometers, CTS, 363S105B, Wavetek P/N 4610-00-1105.


Also, add L1 (Wavetek P/N 1810-05-0004) to the Parts List.
Page 5-14 Figures 5-20 and 5-21 are reversed. Figure 5-20 (M104A Adjustments) is updated as shown. (NOTE: RF Bal and S.S. Bal are factory adjustments.)


Add 10K resistor R43 (Wavetek P/N 4700-15-1002) from pin 2 of IC1 to ground.

M1 06


