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Instruction Manual
for

V.H.F. BRIDGES

TYPES B.701 & B.801

WAYNE KERR LABORATORIES - CHESSINGTON - SURREY



GENERAL

THE WAYNE KERR V.H.F. Admittance Bridges Types B. 701 and B. 801 have been designed for the measurement of aerials, cables and feeders in the frequency range 1 - 100 Mc/s., but are capable of a variety of admittance measurements of components in general.

The bridges possess the following outstanding advantages:-

1. Both balanced and unbalanced impedances can be measured with equal facility.
2. The low impedance to ground and between terminals ensures extreme stability.
3. The employment of the "tapped transformer" principle avoids the difficulties associated with standard elements of large physical size.

SETTING UP THE BRIDGE

Source and Detector

A suitable source is an oscillating or signal generator having an output of approximately 1 V r.m.s. over the required frequency range.

A standard Gommelation Resonator is suitable for coupling takes place between the source and the detector (see Sixty-ninth, below).

detectors, provided that its sensitivity does not fall below 5 microvolts at 100 Mc/s. It is important that no direct connection is made between the source and the detector (see

Wynne Kerr Laboratories.

Suitable sources and detectors can be supplied by

Screening

unless the resonator is extremely good, errors in measurement will be caused by an oscillator and will be magnified by an equal amount to the input to the bridge.

particular, particularly between the unknown and the input to the resonator, and will be magnified by an amount equal to the bridge signal.

Any signal so induced will be picked up by the receiver and will be measured to be balanced when the bridge anti-phase signal from the bridge when balanced. The bridge will therefore be off balance at the null point by an amount equal to the bridge signal.

As it is difficult to screen the unknown adequately, a partioner across should be taken with the input to the detector.

The amount of radiation can be checked when the bridge is connected to the source and detector by stripping the timer conductor from the bridge and turning it so that the bridge is touching the outer shell of the cable plus it is touching the outer insulation of the cable.

It is negligible when the receiver is at full gain.

CONNEXION TO TERMINALS

For measuring components and balanced admittances, the "unknown" is connected across the block terminals with the Earth and Neutral terminals left free.

For measuring unbalanced admittances, the Earth terminal and the block terminal nearest the front panel are connected together by means of the strap provided.

Errors in measurement will occur if other means of earthing are adopted.

B.701 Earth Terminal

A second earth terminal is provided in the B.701 for use when measuring balanced impedances with an "earthy" screen.

B.801 Neutral Terminal

The diagram of Fig. 2 shows the internal connexion of the neutral terminal of the B.801 Bridge. A and B are the normal block terminals, and N is the neutral terminal connected to the neutral line between the transformers.

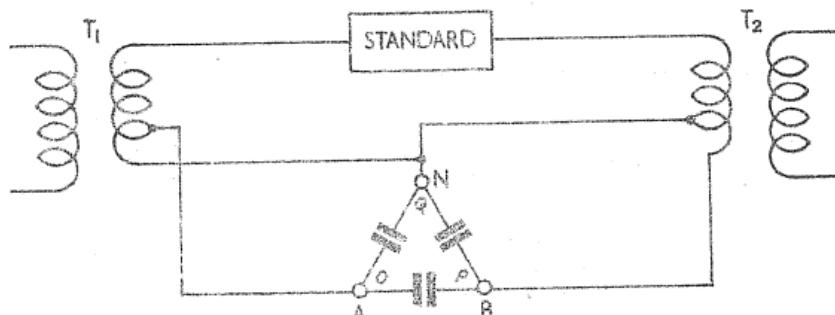


Fig. 2

The Set Zero controls, which are used in the initial balancing of the bridge, are effective in parallel with the main standards and can be used for a linear degree of balance when measuring the unknown.

Use of Set Zero Controls

As the effective value of the strays in the extra-out very little frequency, it is important to re-balance the bridge when the frequency is changed.

The conductance drifts the direct reading and independent of frequency. The susceptance value is found by calibrating the susceptance of the capacitive readings on the main drift at the frequency of measurement.

The ultimate is then connected and the bridge rebalanced, using the main controls.

When making a preliminary balance the detector R.F. gain should be reduced in order to avoid overloading, and the tuning should be adjusted before finally rebalancing and the bridge. (See p. 1).

If the unknown is multivalued, the extra should be connected before carrying out the initial balancing of the bridge.

Having set the source and detector to the pre-
"unknown" to the terminals, with the main controls set to zero before connecting the quantity of measurement required, the bridge is balanced.

MEASUREMENT PROCEDURE

When a component is connected to the bridge with screened leads of approximately length, the sources can be connected together and to the neutral terminal. If the conductance of the measurement required, the bridge is imbalanced to that of the unknown.

If a three-terminal capacity is connected as shown in the figure, the capacities Q-Q and P-Q are effectively in shunt across the transducer and do not affect the balancing of the bridge.

In this case, the difference between the readings is added to the value of the conductance or susceptance on the main dial.

Measurement of R and C

Once the bridge is balanced, the dials give a direct reading of unknown R and C. If the values for the equivalent series circuit of the unknown are required, they can be obtained from the relations:

$$R_s = \frac{R}{1 + (R^2/X^2)} = \frac{R}{1 + \omega^2 C^2 R^2}$$

$$\text{and } X_s = \frac{X}{1 + (X^2/R^2)}, \quad C_s = C + \frac{1}{\omega^2 C R^2}$$

where R_s , C_s , and X_s are the resistance, capacitance, and reactance of the equivalent series circuit and R , C , and X the resistance, capacitance, and reactance of the parallel circuit as measured by the bridge.

Measurement of R and L

The bridge measures values of R and L as a parallel combination, the inductive component being balanced in terms of equivalent negative capacitance, i.e. the value of capacitance which has the same reactance as the unknown at the frequency of measurement.

In order to arrive at the value of inductance the frequency must be known, and the accuracy of measurement is dependent on the accuracy of measurement of the source frequency.

The procedure for measurement is the same as that for the measurement of R and C. After the required earthing connexions have been made, the bridge is balanced and the unknown is connected between the terminals. The bridge is rebalanced on the R and C dials.

The R scale is independent of frequency, and the value of L is calculated as follows:

that on the "unknown" side. If an excess balance is required frequency owing to the loss on the standard side exceeding true loss the B,801 bridge may not balance at extreme high When measuring a capacitor with very low dielectric-

capacitor can be obtained on the B,801 bridge.

with a three-terminal capacitor, a virtually lossless and by making use of the neutral terminal in combination with a three-terminal capacitor, a combination method, final air-dielectric capacitor by the substitution method.

losses can be measured with the aid of an exten-

Measurement of Dielectric Loss

parallel induction is less than 1%.

than 10 the difference between the equivalent series and It should be noted that for values of Q greater

where R, X and L have the same values as before.

$$L_s = \frac{1 + (\omega L^2/R^2)}{L} = \frac{1 + (1/q^2)}{L}$$

$$X_s = \frac{1 + (X^2/R^2)}{X} = \frac{1 + (1/q^2)}{X}$$

$$R_s = \frac{1 + (R^2/X^2)}{R} = \frac{1 + q^2}{R}$$

from the relations:

terms of equivalent series circuit, they can be calculated If the constants of the unknown are required in

Equivalent Series Circuit

resistance of the frequency used.

value of induction having the same From the same resistance chart find the

frequency used.

find the resistance of the capacitor at the chart of resistance (or by calculation) From the reading of the C scale and a

for comparison purposes, it is permissible to obtain it by means of the "Balance R" control, which increases the loss of the unknown side without affecting the capacitance.

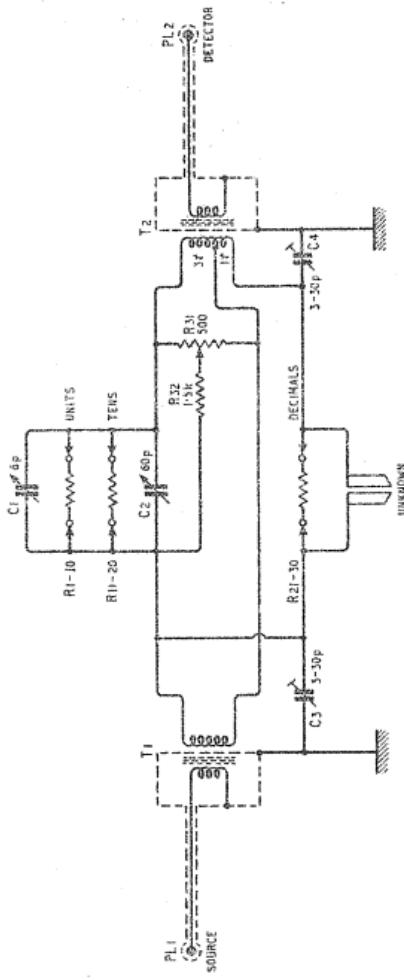
Measurement of Transmission Lines and Aerials.

The bridges will measure accurately the impedance of all transmission lines and aerials, whether unbalanced or balanced. The procedure is the same as that previously described, but it is important that the receiver is adequately screened from the aerial or cable under test.

C. 1		6 pF.	Air Dielectric Triimmer.	Input Transformer to W.K. Dwg. CWP, 3109		
C. 2		60 pF.	Air Dielectric Triimmer.	Internal Standard (W.K.L. Dwg. CWP, 3109)		
C. 3		3-30 pF.	Air Dielectric Triimmer.	Air Dielectric Triimmer,		
R. 1	R. 2	3000	Dummy resistor	+1% -3%	$\frac{1}{2}W$, H.S. Carbon	ohms
R. 3	R. 4	1000	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 5	R. 6	750	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 7	R. 8	500	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 9	R. 10	375	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 11	R. 12	300	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 13	R. 14	150	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 15	R. 16	75	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 17	R. 18	60	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 19	R. 20	50	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 21	R. 22	1000	Dummy resistor	+0 -2%	$\frac{1}{2}W$, H.S. Carbon	
R. 23	R. 24	1250	Dummy resistor	+1% -3%	$\frac{1}{2}W$, H.S. Carbon	
R. 25	R. 26	1667	Dummy resistor	+1% -3%	$\frac{1}{2}W$, H.S. Carbon	
R. 27	R. 28	2000	Dummy resistor	+2 -3%	$\frac{1}{2}W$, H.S. Carbon	
R. 29	R. 30	3333	Dummy resistor	+3 -5%	$\frac{1}{2}W$, H.S. Carbon	
R. 31	R. 32	5000	Dummy resistor	+5 -10%	$\frac{1}{2}W$, H.S. Carbon	
T1		10000	Dummy resistor	+5 -7%	$\frac{1}{2}W$, H.S. Carbon	
T2		50000	Dummy resistor	+5 -10%	$\frac{1}{2}W$, H.S. Carbon	
T3		200000	Dummy resistor	+10% -10%	$\frac{1}{2}W$, H.S. Carbon	

COMPONENT VALUES

V.H.F. BRIDGE B.701



V.H.F. BRIDGE
Type B701

The Wayne Kerr Laboratories Ltd.

DRG NO CD1004

R. 1	4	PF.	Attri Di-electric Triimmer Vermixer G.	C. 2	60	PF.	Interrinal Standard WKL Dwg. QWP, 3110.
R. 1	9000	ohms	Dummy resistor.	C. 3	10	PF.	Air Di-electric Triimmer Vermixer.
R. 2	3000		+3 -5%	C. 4	12	PF.	" "
R. 3	4500		+1 -3%	C. 5	12	PF.	" "
R. 4	3000		+1 -3%	C. 6	5-50	PF.	Adjusted in test.
R. 5	2250		+0 -2%	C. 7	5-20	PF.	" "
R. 6	1800		+0 -2%	C. 8	5-20	PF.	" "
R. 7	1500		+0 -2%	C. 9	1125	PF.	" "
R. 8	1286		+0 -2%	R. 11	1000	PF.	" "
R. 9	1125		+0 -2%	R. 12	900	PF.	Dummy resistor.
R. 10	1000		+0 -2%	R. 13	450	PF.	+5 -7% H.S. Carbon.
R. 11	1000		+0 -2%	R. 14	300	PF.	+3 -5% H.S. Carbon.
R. 12	900		+0 -2%	R. 15	225	PF.	+3 -5% H.S. Carbon.
R. 13	450		+0 -2%	R. 16	180	PF.	+3 -5% H.S. Carbon.
R. 14	300		+0 -2%	R. 17	150	PF.	+3 -5% H.S. Carbon.
R. 15	225		+0 -2%	R. 18	125	PF.	+3 -5% H.S. Carbon.
R. 16	180		+0 -2%	R. 19	112.5	PF.	+3 -5% H.S. Carbon.
R. 17	150		+0 -2%	R. 20	100	PF.	+20% $\frac{1}{2}W$ Carbon Linear
R. 18	125		+0 -2%	R. 21	500	PF.	+5% $\frac{1}{2}W$ H.S. Carbon
R. 19	112.5		+0 -2%	R. 22	112.5	PF.	+20% $\frac{1}{2}W$ Carbon Linear
R. 20	100		+0 -2%	R. 23	150-180	PF.	+20% $\frac{1}{2}W$ Carbon Linear
R. 21	500		+0 -2%	R. 24	500	PF.	+5% $\frac{1}{2}W$ H.S. Carbon
R. 22	112.5		+0 -2%	R. 25	5000	PF.	+5% $\frac{1}{2}W$ H.S. Carbon
R. 23	150-180		+0 -2%				Adjusted in test.
R. 24	500		+0 -2%				Output " " no. QWP111
R. 25	5000		+0 -2%				Input Transformer to WKL Dwg. no. QWP111
							and all Models subsequent to Serial No. 358
							Modifications to SERIAL Nos. 312 to 315, 332 to 342, 350 & 358
							COMPONENT VALUES INCLUDING
							V.H.P. BRIDGE TYPE B.801

Adjusted in test.

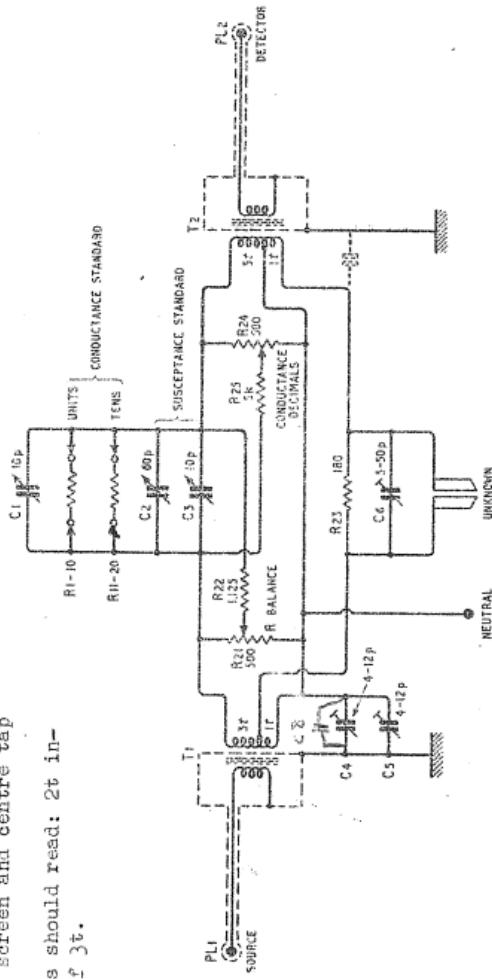
L. 1

MODIFICATIONS

For revised component values,
see opposite page.

Add C8 in parallel with C4.

Add C7 & L1 in series between
earthing screen and centre tap
of T1.
T1 turns should read: 2t in-
stead of 3t.



V.H.F. BRIDGE
Type B801

The Wayne Kerr Laboratories Ltd.

DRG NO CD1005

